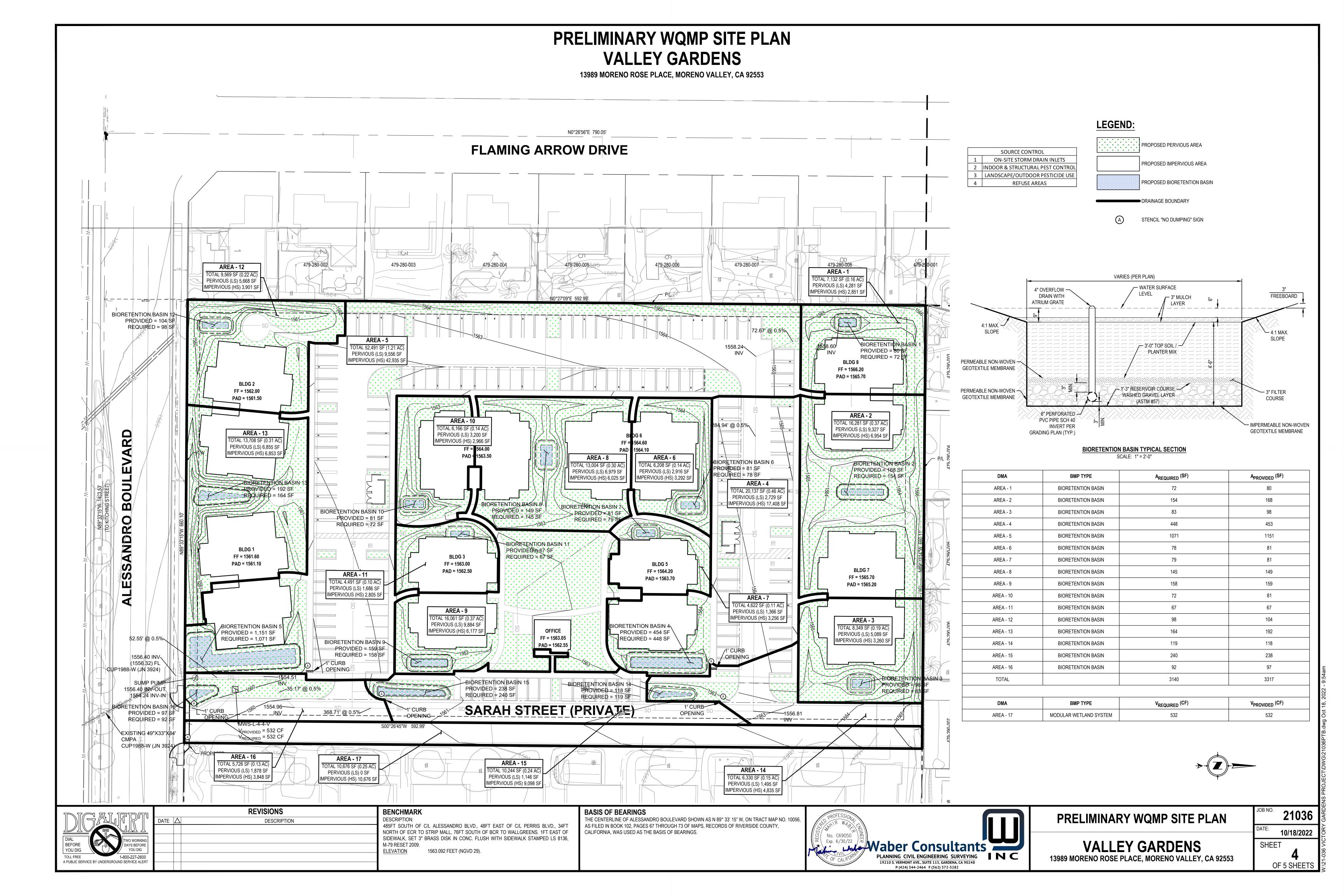
APPENDIX G1 PRELIMINARY WATER QUALITY MANAGEMENT PLAN





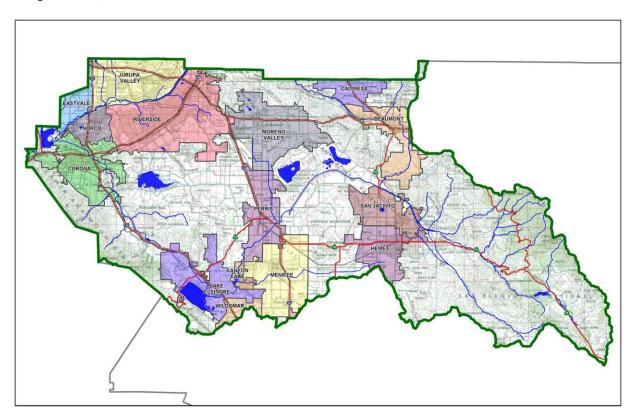
Project Specific Water Quality Management Plan

A Template for Projects located within the **Santa Ana Watershed** Region of Riverside County

Project Title: Valley Gardens

Development No: 13989 Moreno Rose Place, Moreno Valley, CA 92553

Design Review/Case No: LWQ21-0055



✓ Preliminary✓ Final

Original Date Prepared: 09/24/2021

Revision Date(s): 10/21/2022

Prepared for Compliance with

Regional Board Order No. R8-2010-0033

Template revised June 30, 2016

Contact Information:

Prepared for:

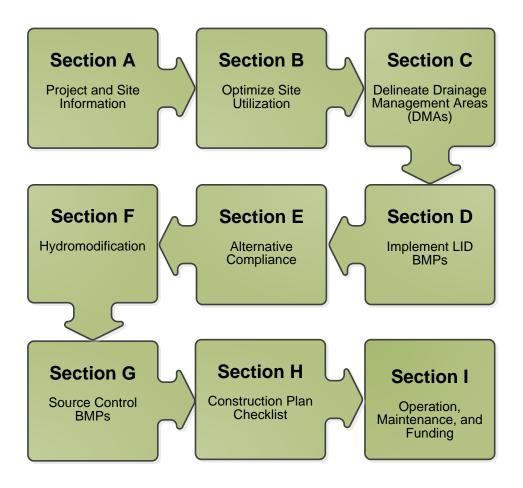
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A Brief Introduction

This Project-Specific WQMP Template for the **Santa Ana Region** has been prepared to help guide you in documenting compliance for your project. Because this document has been designed to specifically document compliance, you will need to utilize the WQMP Guidance Document as your "how-to" manual to help guide you through this process. Both the Template and Guidance Document go hand-in-hand and will help facilitate a well-prepared Project-Specific WQMP. Below is a flowchart for the layout of this Template that will provide the steps required to document compliance.



OWNER'S CERTIFICATION

This Project-Specific Water Quality Management Plan (WQMP) has been prepared for Moreno Valley Garden, LLC by Waber Consultants, Inc. for the Valley Gardens project.

This WQMP is intended to comply with the requirements of City of Moreno Valley for Ordinance No. 827 which includes the requirement for the preparation and implementation of a Project-Specific WQMP.

The undersigned, while owning the property/project described in the preceding paragraph, shall be responsible for the implementation and funding of this WQMP and will ensure that this WQMP is amended as appropriate to reflect up-to-date conditions on the site. In addition, the property owner accepts responsibility for interim operation and maintenance of Stormwater BMPs until such time as this responsibility is formally transferred to a subsequent owner. This WQMP will be reviewed with the facility operator, facility supervisors, employees, tenants, maintenance and service contractors, or any other party (or parties) having responsibility for implementing portions of this WQMP. At least one copy of this WQMP will be maintained at the project site or project office in perpetuity. The undersigned is authorized to certify and to approve implementation of this WQMP. The undersigned is aware that implementation of this WQMP is enforceable under City of Moreno Valley Water Quality Ordinance (Municipal Code Chapter 8.10).

"I, the undersigned, certify under penalty of law that the provisions of this WQMP have been reviewed and accepted and that the WQMP will be transferred to future successors in interest." Owner's Signature Date Owner's Printed Name Owner's Title/Position PREPARER'S CERTIFICATION "The selection, sizing and design of stormwater treatment and other stormwater quality and quantity control measures in this plan meet the requirements of Regional Water Quality Control Board Order No. R8-2010-0033 and any subsequent amendments thereto." 10/21/2022 Date Principal Mahir Waber P.E., QSD Preparer's Printed Name Preparer's Title/Position Preparer's Licensure:

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Section A: Project and Site Information

PROJECT INFORMATION			
Type of Project:	New Development Projects, Parking Lots		
Planning Area:	Valley Gardens		
Community Name:	Valley Gardens		
Development Name:	Valley Gardens		
PROJECT LOCATION			
Latitude & Longitude (DMS):	33.918, -117.221		
Project Watershed and Sub-	Watershed: Santa Ana Watershed		
Gross Acres: 4.85 AC APN(s): 479-220-024			
Map Book and Page No.: Boo	ok 102, Page 67-73		
PROJECT CHARACTERISTICS			
Proposed or Potential Land L	Jse(s)	New	Development
		Projects	s, Parking Lots
Proposed or Potential SIC Co	de(s)	6513	
Area of Impervious Project F	ootprint (SF)	137,140)
Total Area of <u>proposed</u>	Impervious Surfaces within the Project Footprint (SF)/or	137,140	ס
Replacement			
Does the project consist of o	-	<u></u> Y	⊠N
Does the project propose to	construct unpaved roads?	☐ Y	⊠ N
Is the project part of a larger	common plan of development (phased project)?	∐ Y	⊠N
Proposed Conditions:			
	nclude 8 residential apartment buildings with one office. Other		
· ·	sphalt and concrete driveways, hardscape and landscaping. The		
	ion basins for 7 DMAs in the landscape areas in the prosed site.		
Calculations are provided.			
EVICTING SITE CHARACTERISTICS			
EXISTING SITE CHARACTERISTICS	ious Cunfosso within the Duniont limits Footpuint (CF)	21 447	
= -	ious Surfaces within the Project limits Footprint (SF)	21,447	⊠ NI
Is the project located within		☐ Y	⊠ N
If so, identify the Cell numbe		N/A	⊠ NI
	ogic features on the project site?	∏ Υ ⊠ ∨	⊠ N □ N
Is a Geotechnical Report atta		⊠ Y	∐ N
• •	e NRCS soils type(s) present on the site (A, B, C and/or D)	-	
what is the water Quality De	esign Storm Depth for the project?	0.67	
Existing Conditions:			
Existing Conditions:	cated along the north cide of Alessandra Paulavard, east of		
	cated along the north side of Alessandro Boulevard, east of		
_	City of Moreno Valley. The generally rectangular shaped parcel		
	south direction. The site is relatively level with topography		
= = '	north to south on the order of a few feet. The site is currently		
vacant and covered in light v	egetation.		

A.1 Maps and Site Plans

When completing your Project-Specific WQMP, include a map of the local vicinity and existing site. In addition, include all grading, drainage, landscape/plant palette and other pertinent construction plans in Appendix 2. At a **minimum**, your WQMP Site Plan should include the following:

- Drainage Management Areas
- Proposed Structural BMPs
- Drainage Path
- Drainage Infrastructure, Inlets, Overflows
- Source Control BMPs
- Buildings, Roof Lines, Downspouts
- Impervious Surfaces
- Standard Labeling
- BMP Locations (Lat/Long)

Use your discretion on whether or not you may need to create multiple sheets or can appropriately accommodate these features on one or two sheets. Keep in mind that the Co-Permittee plan reviewer must be able to easily analyze your project utilizing this template and its associated site plans and maps.

A.2 Identify Receiving Waters

Using Table A.1 below, list in order of upstream to downstream, the receiving waters that the project site is tributary to. Continue to fill each row with the Receiving Water's 303(d) listed impairments (if any), designated beneficial uses, and proximity, if any, to a RARE beneficial use. Include a map of the receiving waters in Appendix 1.

Table A.1 Identification of Receiving Waters

Receiving Waters	EPA Approved 303(d) List Impairments	Designated Beneficial Uses	Proximity to RARE Beneficial Use	
Santa Ana River, Reach 3	Copper, Lead, Pathogens	N/A	N/A	
Santa Ana River, Reach 2	Indicator Bacteria	N/A	N/A	
Santa Ana River, Reach 1	Fecal Coliform	Secondary Contact, Swimming	40 mile	
Pacific Ocean				

A.3 Additional Permits/Approvals required for the Project:

Table A.2 Other Applicable Permits

Agency	Permit Required	
State Department of Fish and Game, 1602 Streambed Alteration Agreement		⊠N
State Water Resources Control Board, Clean Water Act (CWA) Section 401 Water Quality Cert.		⊠N
US Army Corps of Engineers, CWA Section 404 Permit		⊠N
US Fish and Wildlife, Endangered Species Act Section 7 Biological Opinion	Y	⊠N
Statewide Construction General Permit Coverage	⊠ Y	□N
Statewide Industrial General Permit Coverage	Y	⊠N
Western Riverside MSHCP Consistency Approval (e.g., JPR, DBESP)		⊠N
Other (please list in the space below as required) Grading and building permits from City of Moreno Valley	⊠ Y	N

Section B: Optimize Site Utilization (LID Principles)

Review of the information collected in Section 'A' will aid in identifying the principal constraints on site design and selection of LID BMPs as well as opportunities to reduce imperviousness and incorporate LID Principles into the site and landscape design. For example, **constraints** might include impermeable soils, high groundwater, groundwater pollution or contaminated soils, steep slopes, geotechnical instability, high-intensity land use, heavy pedestrian or vehicular traffic, utility locations or safety concerns. **Opportunities** might include existing natural areas, low areas, oddly configured or otherwise unbuildable parcels, easements and landscape amenities including open space and buffers (which can double as locations for bioretention BMPs), and differences in elevation (which can provide hydraulic head). Prepare a brief narrative for each of the site optimization strategies described below. This narrative will help you as you proceed with your LID design and explain your design decisions to others.

The 2010 Santa Ana MS4 Permit further requires that LID Retention BMPs (Infiltration Only or Harvest and Use) be used unless it can be shown that those BMPs are infeasible. Therefore, it is important that your narrative identify and justify if there are any constraints that would prevent the use of those categories of LID BMPs. Similarly, you should also note opportunities that exist which will be utilized during project design. Upon completion of identifying Constraints and Opportunities, include these on your WQMP Site plan in Appendix 1.

Consideration of "highest and best use" of the discharge should also be considered. For example, Lake Elsinore is evaporating faster than runoff from natural precipitation can recharge it. Requiring infiltration of 85% of runoff events for projects tributary to Lake Elsinore would only exacerbate current water quality problems associated with Pollutant concentration due to lake water evaporation. In cases where rainfall events have low potential to recharge Lake Elsinore (i.e. no hydraulic connection between groundwater to Lake Elsinore, or other factors), requiring infiltration of Urban Runoff from projects is counterproductive to the overall watershed goals. Project proponents, in these cases, would be allowed to discharge Urban Runoff, provided they used equally effective filtration-based BMPs.

Site Optimization

The following questions are based upon Section 3.2 of the WQMP Guidance Document. Review of the WQMP Guidance Document will help you determine how best to optimize your site and subsequently identify opportunities and/or constraints, and document compliance.

Did you identify and preserve existing drainage patterns? If so, how? If not, why?

Yes, the proposed site will preserve existing site drainage patterns. The proposed drainage pattern for the site is in a southeasternly direction matching the existing drainage pattern.

Did you identify and protect existing vegetation? If so, how? If not, why?

No, there are no significant trees and other natural vegetation needed to be preserved. The site is barren.

Did you identify and preserve natural infiltration capacity? If so, how? If not, why?

Yes, even though the infiltration rate at the depths tested indicate stiff/dense soils which are not suitable for storm water infiltration, infiltration for the proposed landscape areas will be persevered. Landscape areas will not be compacted.

Did you identify and minimize impervious area? If so, how? If not, why?

Yes, the site has been designed with the idea of minimizing impervious areas. The site is designed with landscaping provided along the north, west and south boundaries and along the building and parking space areas which totally contribute to 32.5% of the total site area compared to typical new developments which have a pervious area of around 10%

Did you identify and disperse runoff to adjacent pervious areas? If so, how? If not, why?

Yes, runoff is designed to drain into landscape areas and into the bioretention facilities.

Section C: Delineate Drainage Management Areas (DMAs)

Utilizing the procedure in Section 3.3 of the WQMP Guidance Document which discusses the methods of delineating and mapping your project site into individual DMAs, complete Table C.1 below to appropriately categorize the types of classification (e.g., Type A, Type B, etc.) per DMA for your project site. Upon completion of this table, this information will then be used to populate and tabulate the corresponding tables for their respective DMA classifications.

Table C.1 DMA Classifications

Bioretention Basin #13	Ornamental		
	Landscaping		
Area – 14	Concrete or Asphalt,		D
Bioretention Basin #14	Ornamental		
	Landscaping	6,330	
Area – 15	Concrete or Asphalt,		D
Bioretention Basin #15	Ornamental		
	Landscaping	10,244	
Area – 16	Concrete or Asphalt,		D
Bioretention Basin #16	Ornamental		
	Landscaping	5,726	
Area – 17	Concrete or Asphalt,		D
Modular Wetland	Ornamental		
System		10,676	

¹Reference Table 2-1 in the WQMP Guidance Document to populate this column

Table C.2 Type 'A', Self-Treating Areas

DMA Name or ID	Area (Sq. Ft.)	Stabilization Type	Irrigation Type (if any)

Table C.3 Type 'B', Self-Retaining Areas

Table C.3 Ty	Table C.3 Type 'B', Self-Retaining Areas					
Self-Retai	ning Area			Type 'C' DM <i>i</i> Area	As that are drain	ing to the Self-Retaining
DMA Name/ ID	Post-project surface type	Area	Storm Depth (inches)	DMA Name /		Required Retention Depth (inches) [D]

$$[D] = [B] + \frac{[B] \cdot [C]}{[A]}$$

Table C.4 Type 'C', Areas that Drain to Self-Retaining Areas

C	DMA	Receiving Self-Retaining DMA

²If multi-surface provide back-up

DMA Name/ ID	Area (square feet)	Post-project surface type	 Product [C] = [A] x [B]	DMA name /ID	Ratio [C]/[D]

Table C.5 Type 'D'. Areas Draining to BMPs

Table C.5 Type D , Areas Draining to BMPS				
DMA Name or ID	BMP Name or ID			
Area – 1	Bioretention Basin #1			
Area – 2	Bioretention Basin #2			
Area – 3	Bioretention Basin #3			
Area – 4	Bioretention Basin #4			
Area – 5	Bioretention Basin #5			
Area – 6	Bioretention Basin #6			
Area – 7	Bioretention Basin #7			
Area – 8	Bioretention Basin #8			
Area – 9	Bioretention Basin #9			
Area – 10	Bioretention Basin #10			
Area – 11	Bioretention Basin #11			
Area – 12	Bioretention Basin #12			
Area – 13	Bioretention Basin #13			
Area – 14	Bioretention Basin #14			
Area – 15	Bioretention Basin #15			
Area – 16	Bioretention Basin #16			
Area – 17	Modular Wetland System			

<u>Note</u>: More than one drainage management area can drain to a single LID BMP, however, one drainage management area may not drain to more than one BMP.

Section D: Implement LID BMPs

D.1 Infiltration Applicability

Is there an approved downstream 'Highest and Best Use' for stormwater runoff (see discussion in Chapter 2.4.4 of the WQMP Guidance Document for further details)? \square Y \bowtie N

If yes has been checked, Infiltration BMPs shall not be used for the site; proceed to section D.3

If no, continue working through this section to implement your LID BMPs. It is recommended that you contact your Co-Permittee to verify whether or not your project discharges to an approved downstream 'Highest and Best Use' feature.

Geotechnical Report

A Geotechnical Report or Phase I Environmental Site Assessment may be required by the Co-Permittee to confirm present and past site characteristics that may affect the use of Infiltration BMPs. In addition, the Co-Permittee, at their discretion, may not require a geotechnical report for small projects as described in Chapter 2 of the WQMP Guidance Document. If a geotechnical report has been prepared, include it in Appendix 3. In addition, if a Phase I Environmental Site Assessment has been prepared, include it in Appendix 4.

Is this project classified as a small project consistent with the requirements of Chapter 2 of the WQMP Guidance Document?

Y

N

Infiltration Feasibility

Table D.1 below is meant to provide a simple means of assessing which DMAs on your site support Infiltration BMPs and is discussed in the WQMP Guidance Document in Chapter 2.4.5. Check the appropriate box for each question and then list affected DMAs as applicable. If additional space is needed, add a row below the corresponding answer.

Table D.1 Infiltration Feasibility

Does the project site	YES	NO
have any DMAs with a seasonal high groundwater mark shallower than 10 feet?		Х
If Yes, list affected DMAs:		
have any DMAs located within 100 feet of a water supply well?		Χ
If Yes, list affected DMAs:		
have any areas identified by the geotechnical report as posing a public safety risk where infiltration of stormwater could have a negative impact?		Х
If Yes, list affected DMAs:		
have measured in-situ infiltration rates of less than 1.6 inches / hour?	Χ	
If Yes, list affected DMAs: Areas 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16 and 17.		
have significant cut and/or fill conditions that would preclude in-situ testing of infiltration rates at the final infiltration surface?		Х
If Yes, list affected DMAs:		
geotechnical report identify other site-specific factors that would preclude effective and safe infiltration?		Χ
Describe here:		

D.2 Harvest and Use Assessment

Please check what applies:

\square Reclaimed water will be used for the non-potable water demands for the project.
\Box Downstream water rights may be impacted by Harvest and Use as approved by the Regional Board (verify with the Copermittee).
☐ The Design Capture Volume will be addressed using Infiltration Only BMPs. In such a case, Harvest and Use BMPs are still encouraged, but it would not be required if the Design Capture Volume will be infiltrated or evapotranspired.

If any of the above boxes have been checked, Harvest and Use BMPs need not be assessed for the site. If none of the above criteria applies, follow the steps below to assess the feasibility of irrigation use, toilet use and other non-potable uses (e.g., industrial use).

Irrigation Use Feasibility

Complete the following steps to determine the feasibility of harvesting stormwater runoff for Irrigation Use BMPs on your site:

Step 1: Identify the total area of irrigated landscape on the site, and the type of landscaping used.

Total Area of Irrigated Landscape: 1.71 AC

Type of Landscaping (Conservation Design or Active Turf): Conservation Design

Step 2: Identify the planned total of all impervious areas on the proposed project from which runoff might be feasibly captured and stored for irrigation use. Depending on the configuration of buildings and other impervious areas on the site, you may consider the site as a whole, or parts of the site, to evaluate reasonable scenarios for capturing and storing runoff and directing the stored runoff to the potential use(s) identified in Step 1 above.

Total Area of Impervious Surfaces: 3.27 AC

Step 3: Cross reference the Design Storm depth for the project site (see Exhibit A of the WQMP Guidance Document) with the left column of Table 2-3 in Chapter 2 to determine the minimum area of Effective Irrigated Area per Tributary Impervious Area (EIATIA).

Enter your EIATIA factor: 1.05

Step 4: Multiply the unit value obtained from Step 3 by the total of impervious areas from Step 2 to develop the minimum irrigated area that would be required.

Minimum required irrigated area: 3.43 AC

Step 5: Determine if harvesting stormwater runoff for irrigation use is feasible for the project by comparing the total area of irrigated landscape (Step 1) to the minimum required irrigated area (Step 4).

Minimum required irrigated area (Step 4)	Available Irrigated Landscape (Step 1)
3.43 AC	1.58 AC

Toilet Use Feasibility

Complete the following steps to determine the feasibility of harvesting stormwater runoff for toilet flushing uses on your site:

Step 1: Identify the projected total number of daily toilet users during the wet season, and account for any periodic shutdowns or other lapses in occupancy:

Projected Number of Daily Toilet Users: 128

Project Type: Residential

Step 2: Identify the planned total of all impervious areas on the proposed project from which runoff might be feasibly captured and stored for toilet use. Depending on the configuration of buildings and other impervious areas on the site, you may consider the site as a whole, or parts of the site, to evaluate reasonable scenarios for capturing and storing runoff and directing the stored runoff to the potential use(s) identified in Step 1 above.

Total Area of Impervious Surfaces: 3.27 AC

Step 3: Enter the Design Storm depth for the project site (see Exhibit A) into the left column of Table 2-2 in Chapter 2 to determine the minimum number or toilet users per tributary impervious acre (TUTIA).

Enter your TUTIA factor: 108

Step 4: Multiply the unit value obtained from Step 3 by the total of impervious areas from Step 2 to develop the minimum number of toilet users that would be required.

Minimum number of toilet users: 353

Step 5: Determine if harvesting stormwater runoff for toilet flushing use is feasible for the project by comparing the Number of Daily Toilet Users (Step 1) to the minimum required number of toilet users (Step 4).

Minimum required Toilet Users (Step 4)	Projected number of toilet users (Step 1)
353	128

Other Non-Potable Use Feasibility

Are there other non-potable uses for stormwater runoff on the site (e.g. industrial use)? See Chapter 2 of the Guidance for further information. If yes, describe below. If no, write N/A.

N/A

Step 1: Identify the projected average daily non-potable demand, in gallons per day, during the wet season and accounting for any periodic shutdowns or other lapses in occupancy or operation.

Average Daily Demand: N/A

Step 2: Identify the planned total of all impervious areas on the proposed project from which runoff might be feasibly captured and stored for the identified non-potable use. Depending on the configuration of buildings and other impervious areas on the site, you may consider the site as a whole, or parts of the site, to evaluate reasonable scenarios for capturing and storing runoff and directing the stored runoff to the potential use(s) identified in Step 1 above.

Total Area of Impervious Surfaces: N/A

Step 3: Enter the Design Storm depth for the project site (see Exhibit A) into the left column of Table 2-4 in Chapter 2 to determine the minimum demand for non-potable uses per tributary impervious acre.

Enter the factor from Table 2-4: N/A

Step 4: Multiply the unit value obtained from Step 3 by the total of impervious areas from Step 2 to develop the minimum number of gallons per day of non-potable use that would be required.

Minimum required use: N/A

Step 5: Determine if harvesting stormwater runoff for other non-potable use is feasible for the project by comparing the projected average daily use (Step 1) to the minimum required non-potable use (Step 4).

Minimum required non-potable use (Step 4)	Projected average daily use (Step 1)
N/A	N/A

If Irrigation, Toilet and Other Use feasibility anticipated demands are less than the applicable minimum values, Harvest and Use BMPs are not required and you should proceed to utilize LID Bioretention and Biotreatment per Section 3.4.2 of the WQMP Guidance Document.

D.3 Bioretention and Biotreatment Assessment

Other LID Bioretention and Biotreatment BMPs as described in Chapter 2.4.7 of the WQMP Guidance Document are feasible on nearly all development sites with sufficient advance planning.

Select one of the following:

⊠ LIC) Bioreter	ntion/Bio	treatmer	t BMP	s will	be	used	for	some	or	all	DMAs	of the	e pro	ject a	as
าoted	below in	Section	D.4 (not	e the	requi	rem	ents	of S	ection	3.4	.2	in the	WQM	ΡGι	ıidano	ce
Docur	nent).															

☐ A site-specific analysis demonstrating the technical infeasibility of all LID BMPs has been performed and is included in Appendix 5. If you plan to submit an analysis demonstrating the technical infeasibility of LID BMPs, request a pre-submittal meeting with the Co-permittee to discuss this option. Proceed to Section E to document your alternative compliance measures.

D.4 Feasibility Assessment Summaries

From the Infiltration, Harvest and Use, Bioretention and Biotreatment Sections above, complete Table D.2 below to summarize which LID BMPs are technically feasible, and which are not, based upon the established hierarchy.

Table D.2 LID Prioritization Summary Matrix

	PHOTILIZACION SUITI		P Hierarchy		No LID
DMA Name/ID	1. Infiltration	2. Harvest and use	3. Bioretention	4. Biotreatment	(Alternative Compliance)
Area - 1			\boxtimes		
Area - 2			\boxtimes		
Area - 3			\boxtimes		
Area - 4					
Area –5			\boxtimes		
Area –6			\boxtimes		
Area - 7			\boxtimes		
Area - 8			\boxtimes		
Area - 9			\boxtimes		
Area – 10			\boxtimes		
Area – 11			\boxtimes		
Area –12			\boxtimes		
Area –13			\boxtimes		
Area - 14			\boxtimes		
Area –15			\boxtimes		
Area - 16			\boxtimes		
Area - 16					

The proposed site will include 8, 2-storey residential buildings. According to the Riverside County Guidance Document Section 2.4.5, LID Infiltration BMPs are not to be used when infiltration rate for the site is less than 1.6 inches per hour. The infiltration rate measured was 0.20 inch per hour. Therefore, infiltration is not feasible at the site.

The available irrigated landscape has been measured to be 1.71 acres which is below the minimum required irrigated area which is determined to be 3.30 acres. Therefore, Harvest and Use is not feasible.

Bioretention basins with underdrains are provided as BMPs for all the DMAs. WQMP site plan provides locations and sizing of each bioretention BMP in each DMA.

D.5 LID BMP Sizing

Each LID BMP must be designed to ensure that the Design Capture Volume will be addressed by the selected BMPs. First, calculate the Design Capture Volume for each LID BMP using the V_{BMP} worksheet in Appendix F of the LID BMP Design Handbook. Second, design the LID BMP to meet the required V_{BMP} using a method approved by the Co-Permittee. Utilize the worksheets found in the LID BMP Design Handbook or consult with your Co-Permittee to assist you in correctly sizing your LID BMPs. Complete Table D.3 below to document the Design Capture Volume and the Proposed Volume for each LID BMP. Provide the completed design procedure sheets for each LID BMP in Appendix 6. You may add additional rows to the table below as needed.

Table D.3 DCV Calculations for LID BMPs

DMA Type/ID	DMA Area (square feet)	Post- Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor [A] x [C]	Design Storm Depth (in)	Design Capture Volume, VBMP (cubic feet)	Proposed Volume on Plans (cubic feet)
AREA - 1 Bioretention Basin #1	7,132	Mixed Surface Types	0.46	0.31	2,243.1	0.67	125.2	140
Total	7,132				2,243.1		125.2	140

DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic	Propos ed Volum e on Plans
	[A]		[B]	[C]	[A] x [C]		feet)	(cubic feet)
AREA – 2 Bioretention Basin #2	16,281	Mixed Surface Types	0.427	0.30	4,804. 2	0.67	268.2	294
Total	16,281				4,804.2		268.2	294

DMA Type/ID	DMA Area (square feet)	Post- Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor [A] x [C]	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
AREA - 3 Bioretention Basin #3	8,349	Mixed Surface Types	0.451	0.31	2,580.9	0.67	144.1	171.5
Total	8,349				2,580.9		144.1	171.5

DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor [A] x [C]	Design Storm Depth (in)	Design Capture Volume , V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
AREA – 4 Bioretention Basin #4	20,137	Mixed Surface Types	0.878	0.70	14,075 .9	0.67	785.9	799
Total	20,137				14,075. 9		785.9	799

DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic feet)	Propos ed Volum e on Plans (cubic feet)
AREA – 5 Bioretention Basin #5	52,491	Mixed Surface Types	0.836	0.64	33,764	0.67	1,885.2	2,025
Total	52,491				33,764		1,885.2	2,025

DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor [A] x [C]	Design Storm Depth (in)	Design Capture Volume , V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
AREA – 6 Bioretention Basin #6	6,208	Mixed Surface Types	0.577	0.39	2,431. 9	0.67	135.8	141.75
Total	6,208				2,431.9		135.8	141.75

DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor [A] x [C]	Design Storm Depth (in)	Design Capture Volume , V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
AREA – 7 Bioretention Basin #7	4,622	Mixed Surface Types	0.734	0.53	2,436. 6	0.67	136	141
Total	4,622				2,436.6		136	141

DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor [A] x [C]	Design Storm Depth (in)	Design Capture Volume , V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
AREA – 8 Bioretention Basin #8	13,004	Mixed Surface Types	0.517	0.35	<i>4,554.</i> <i>5</i>	0.67	254.3	262
Total	13,004				4,554.5		254.3	262

DMA Type/ID	DMA Area (square feet) [A]	Post-Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor [A] x [C]	Design Storm Depth (in)	Design Capture Volume , V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
AREA – 9 Bioretention Basin #9	16,061	Mixed Surface Types	0.446	0.31	4,917. 4	0.67	274.6	278
Total	16,061				4,917.4	-	274.6	278

DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor [A] x [C]	Design Storm Depth (in)	Design Capture Volume , V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
AREA – 10 Bioretention Basin #10	6,166	Mixed Surface Types	0.533	0.36	2,225. 1	0.67	124.2	141.75
Total	6,166				2,225.1		124.2	141.75

DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume , V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
AREA – 11 Bioretention Basin #11	4,491	Mixed Surface Types	0.662	0.46	<i>2,063.</i> 5	0.67	115.2	115.3
Total	4,491				2,063.5		115.2	115.3

DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor [A] x [C]	Design Storm Depth (in)	Design Capture Volume , V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
AREA – 12 Bioretention Basin #12	9,569	Mixed Surface Types	0.467	0.32	3,050	0.67	170.3	182
Total	9,569	_			3,050	-	170.3	182

DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor [A] x [C]	Design Storm Depth (in)	Design Capture Volume , V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
AREA – 13 Bioretention Basin #13	13,708	Mixed Surface Types	0.55	0.37	5,106. 2	0.67	285.1	336
Total	13,708				5,106.2		285.1	336

DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor [A] x [C]	Design Storm Depth (in)	Design Capture Volume , V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
AREA – 14 Bioretention Basin #14	6,330	Mixed Surface Types	0.787	0.58	3,698. 3	0.67	206.5	206.5
Total	6,330				3,698.3	_	206.5	206.5

DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor [A] x [C]	Design Storm Depth (in)	Design Capture Volume , V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
AREA – 15 Bioretention Basin #15	10,244	Mixed Surface Types	0.899	0.73	7,466. 1	0.67	416.9	414
Total	10,244				7,466.1		416.9	414

DMA Type/ID	DMA Area (square feet) [A]	Post-Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor [A] x [C]	Design Storm Depth (in)	Design Capture Volume , V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
AREA – 16 Bioretention Basin #16	5,726	Mixed Surface Types	0.705	0.50	2,855. 2	0.67	159.4	169
Total	5,726				2,855.2		159.4	169

DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor [A] x [C]	Design Storm Depth (in)	Design Capture Volume , V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
AREA – 17 Modular Wetland System	10,676	Concrete or Asphalt	1	0.89	9,523	0.67	531.7	532
Total	10,676				9,523		531.7	532

[[]B], [C] is obtained as described in Section 2.3.1 of the WQMP Guidance Document

$$V_{BMP}(ft^3) = \frac{[A] \times [B]}{12 (in/ft)}$$

[[]E] is obtained from Exhibit A in the WQMP Guidance Document

[[]G] is obtained from a design procedure sheet, such as in LID BMP Design Handbook and placed in Appendix 6

Section E: Alternative Compliance (LID Waiver Program)

LID BMPs are expected to be feasible on virtually all projects. Where LID BMPs have been demonstrated to be infeasible as documented in Section D, other Treatment Control BMPs must be used (subject to LID waiver approval by the Co-Permittee). Check one of the following Boxes:

☑ LID Principles and LID BMPs have been incorporated into the site design to fully address all Drainage Management Areas. No alternative compliance measures are required for this project and thus this Section is not required to be completed.

- Or -

☐ The following Drainage Management Areas are unable to be addressed using LID BMPs. A site-specific analysis demonstrating technical infeasibility of LID BMPs has been approved by the Co-Permittee and included in Appendix 5. Additionally, no downstream regional and/or subregional LID BMPs exist or are available for use by the project. The following alternative compliance measures on the following pages are being implemented to ensure that any pollutant loads expected to be discharged by not incorporating LID BMPs, are fully mitigated.

E.1 Identify Pollutants of Concern

Utilizing Table A.1 from Section A above which noted your project's receiving waters and their associated EPA approved 303(d) listed impairments, cross reference this information with that of your selected Priority Development Project Category in Table E.1 below. If the identified General Pollutant Categories are the same as those listed for your receiving waters, then these will be your Pollutants of Concern and the appropriate box or boxes will be checked on the last row. The purpose of this is to document compliance and to help you appropriately plan for mitigating your Pollutants of Concern in lieu of implementing LID BMPs.

Table E.1 Potential Pollutants by Land Use Type

Prior		t General Pollutant Categories							
Project Categories and/or Project Features (check those that apply)		Bacterial Indicators	Metals	Nutrients	Pesticides	Toxic Organic Compounds	Sediments	Trash & Debris	Oil & Grease
	Detached Residential Development	Р	N	Р	Р	N	Р	Р	Р
\boxtimes	Attached Residential Development	Р	N	Р	Р	N	Р	Р	P ⁽²⁾
	Commercial/Industrial Development	P ⁽³⁾	Р	P ⁽¹⁾	P ⁽¹⁾	P ⁽⁵⁾	P ⁽¹⁾	Р	Р
	Automotive Repair Shops	N	Р	N	N	P ^(4, 5)	N	Р	Р
	Restaurants (>5,000 ft ²)	Р	N	N	N	N	N	Р	Р
	Hillside Development (>5,000 ft²)	Р	N	Р	Р	N	Р	Р	Р
\boxtimes	Parking Lots (>5,000 ft²)	P ⁽⁶⁾	Р	P ⁽¹⁾	P ⁽¹⁾	P ⁽⁴⁾	P ⁽¹⁾	Р	Р
	Retail Gasoline Outlets	N	Р	N	N	Р	N	Р	Р
Project Priority Pollutant(s) of Concern									

P = Potential

N = Not Potential

⁽¹⁾ A potential Pollutant if non-native landscaping exists or is proposed onsite; otherwise not expected

⁽²⁾ A potential Pollutant if the project includes uncovered parking areas; otherwise not expected

⁽³⁾ A potential Pollutant is land use involving animal waste

⁽⁴⁾ Specifically petroleum hydrocarbons

⁽⁵⁾ Specifically solvents

⁽⁶⁾ Bacterial indicators are routinely detected in pavement runoff

E.2 Stormwater Credits

Projects that cannot implement LID BMPs but nevertheless implement smart growth principles are potentially eligible for Stormwater Credits. Utilize Table 3-8 within the WQMP Guidance Document to identify your Project Category and its associated Water Quality Credit. If not applicable, write N/A.

Table E.2 Water Quality Credits

Qualifying Project Categories	Credit Percentage ²	
Higher density development	5%	
Total Credit Percentage ¹	5%	

¹Cannot Exceed 50%

E.3 Sizing Criteria

After you appropriately considered Stormwater Credits for your project, utilize Table E.3 below to appropriately size them to the DCV, or Design Flow Rate, as applicable. Please reference Chapter 3.5.2 of the WQMP Guidance Document for further information.

Table E.3 Treatment Control BMP Sizing

DMA Type/ID	DMA Area (square feet) [A]	Post- Project Surface Type	Effective Impervious Fraction, I _f	DMA Runoff Factor	DMA Area x Runoff Factor [A] x [C]		Enter BMP Na	me / Identifiel	r Here
						Design Storm Depth (in)	Minimum Design Capture Volume or Design Flow Rate (cubic feet or cfs)	Total Storm Water Credit % Reduction	Proposed Volume or Flow on Plans (cubic feet or cfs)
_	A _T = Σ[A]				Σ= [D]	[E]	$[F] = \frac{[D]x[E]}{[G]}$	[F] X (1-[H])	[1]

[[]B], [C] is obtained as described in Section 2.3.1 from the WQMP Guidance Document

 $^{^2}$ Obtain corresponding data from Table 3-8 in the WQMP Guidance Document

[[]E] is for Flow-Based Treatment Control BMPs [E] = .2, for Volume-Based Control Treatment BMPs, [E] obtained from Exhibit A in the WQMP Guidance Document

[[]G] is for Flow-Based Treatment Control BMPs [G] = 43,560, for Volume-Based Control Treatment BMPs, [G] = 12

[[]H] is from the Total Credit Percentage as Calculated from Table E.2 above

[[]I] as obtained from a design procedure sheet from the BMP manufacturer and should be included in Appendix 6

E.4 Treatment Control BMP Selection

Treatment Control BMPs typically provide proprietary treatment mechanisms to treat potential pollutants in runoff, but do not sustain significant biological processes. Treatment Control BMPs must have a removal efficiency of a medium or high effectiveness as quantified below:

- **High**: equal to or greater than 80% removal efficiency
- Medium: between 40% and 80% removal efficiency

Such removal efficiency documentation (e.g., studies, reports, etc.) as further discussed in Chapter 3.5.2 of the WQMP Guidance Document, must be included in Appendix 6. In addition, ensure that proposed Treatment Control BMPs are properly identified on the WQMP Site Plan in Appendix 1.

Table E.4 Treatment Control BMP Selection

Selected Treatment Control BMP Name or ID ¹	Priority Pollutant(s) of Concern to Mitigate ²	Removal Efficiency Percentage ³

¹ Treatment Control BMPs must not be constructed within Receiving Waters. In addition, a proposed Treatment Control BMP may be listed more than once if they possess more than one qualifying pollutant removal efficiency.

² Cross Reference Table E.1 above to populate this column.

³ As documented in a Co-Permittee Approved Study and provided in Appendix 6.

Section F: Hydromodification

F.1 Hydrologic Conditions of Concern (HCOC) Analysis

Once you have determined that the LID design is adequate to address water quality requirements, you will need to assess if the proposed LID Design may still create a HCOC. Review Chapters 2 and 3 (including Figure 3-7) of the WQMP Guidance Document to determine if your project must mitigate for Hydromodification impacts. If your project meets one of the following criteria which will be indicated by the check boxes below, you do not need to address Hydromodification at this time. However, if the project does not qualify for Exemptions 1, 2 or 3, then additional measures must be added to the design to comply with HCOC criteria. This is discussed in further detail below in Section F.2.

HCOC EXEMPTION 1 : The Priority Development Project disturbs less than one acre. The Co Permittee has the discretion to require a Project-Specific WQMP to address HCOCs on projects less than one acre on a case by case basis. The disturbed area calculation should include all disturbances associated with larger common plans of development.
Does the project qualify for this HCOC Exemption?
If Yes, HCOC criteria do not apply.
HCOC EXEMPTION 2 : The volume and time of concentration ¹ of storm water runoff for the post development condition is not significantly different from the pre-development condition for a 2-yea return frequency storm (a difference of 5% or less is considered insignificant) using one of the following methods to calculate:
Riverside County Hydrology Manual
 Technical Release 55 (TR-55): Urban Hydrology for Small Watersheds (NRCS 1986), o derivatives thereof, such as the Santa Barbara Urban Hydrograph Method
Other methods acceptable to the Co-Permittee
Does the project qualify for this HCOC Exemption?
If Yes, report results in Table F.1 below and provide your substantiated hydrologic analysis in Appendix 7.
Table F.1 Hydrologic Conditions of Concern Summary

Post-condition

% Difference

2 year – 24 hour Pre-condition

Time of Concentration

Volume (Cubic Feet)

¹ Time of concentration is defined as the time after the beginning of the rainfall when all portions of the drainage basin are contributing to flow at the outlet.

HCOC EXEMPTION 3: All downstream conveyance channels to an adequate sump (for example, Prado Dam, Lake Elsinore, Canyon Lake, Santa Ana River, or other lake, reservoir or naturally erosion resistant feature) that will receive runoff from the project are engineered and regularly maintained to ensure design flow capacity; no sensitive stream habitat areas will be adversely affected; or are not identified on the Co-Permittees Hydromodification Susceptibility Maps.

Does the project qualify for this HCOC Exemption?	⊠ Y □ N
If Yes, HCOC criteria do not apply and note below qualifier:	which adequate sump applies to this HCOO

The proposed site will eventually channel to Canyon Lake. According to the Riverside County-Santa Ana Region Watershed Action Plan Appendix A — Map 1, the site will drain to adequate sumps that are engineered and regularly maintained. The project will limit the disturbance of natural waterbodies and drainage systems and conserve natural areas to maintain the biological integrity of natural waterbodies and drainage systems. Permanent measures will also be provided to reduce the pollutant loads from the development site.

F.2 HCOC Mitigation

If none of the above HCOC Exemption Criteria are applicable, HCOC criteria is considered mitigated if they meet one of the following conditions:

- a. Additional LID BMPS are implemented onsite or offsite to mitigate potential erosion or habitat impacts as a result of HCOCs. This can be conducted by an evaluation of site-specific conditions utilizing accepted professional methodologies published by entities such as the California Stormwater Quality Association (CASQA), the Southern California Coastal Water Research Project (SCCRWP), or other Co-Permittee approved methodologies for site-specific HCOC analysis.
- b. The project is developed consistent with an approved Watershed Action Plan that addresses HCOC in Receiving Waters.
- c. Mimicking the pre-development hydrograph with the post-development hydrograph, for a 2-year return frequency storm. Generally, the hydrologic conditions of concern are not significant, if the post-development hydrograph is no more than 10% greater than pre-development hydrograph. In cases where excess volume cannot be infiltrated or captured and reused, discharge from the site must be limited to a flow rate no greater than 110% of the pre-development 2-year peak flow.

Be sure to include all pertinent documentation used in your analysis of the items a, b or c in Appendix 7.

Section G: Source Control BMPs

Source control BMPs include permanent, structural features that may be required in your project plans — such as roofs over and berms around trash and recycling areas — and Operational BMPs, such as regular sweeping and "housekeeping", that must be implemented by the site's occupant or user. The MEP standard typically requires both types of BMPs. In general, Operational BMPs cannot be substituted for a feasible and effective permanent BMP. Using the Pollutant Sources/Source Control Checklist in Appendix 8, review the following procedure to specify Source Control BMPs for your site:

- 1. *Identify Pollutant Sources*: Review Column 1 in the Pollutant Sources/Source Control Checklist. Check off the potential sources of Pollutants that apply to your site.
- 2. **Note Locations on Project-Specific WQMP Exhibit:** Note the corresponding requirements listed in Column 2 of the Pollutant Sources/Source Control Checklist. Show the location of each Pollutant source and each permanent Source Control BMP in your Project-Specific WQMP Exhibit located in Appendix 1.
- 3. Prepare a Table and Narrative: Check off the corresponding requirements listed in Column 3 in the Pollutant Sources/Source Control Checklist. In the left column of Table G.1 below, list each potential source of runoff Pollutants on your site (from those that you checked in the Pollutant Sources/Source Control Checklist). In the middle column, list the corresponding permanent, Structural Source Control BMPs (from Columns 2 and 3 of the Pollutant Sources/Source Control Checklist) used to prevent Pollutants from entering runoff. Add additional narrative in this column that explains any special features, materials or methods of construction that will be used to implement these permanent, Structural Source Control BMPs.
- 4. Identify Operational Source Control BMPs: To complete your table, refer once again to the Pollutant Sources/Source Control Checklist. List in the right column of your table the Operational BMPs that should be implemented as long as the anticipated activities continue at the site. Copermittee stormwater ordinances require that applicable Source Control BMPs be implemented; the same BMPs may also be required as a condition of a use permit or other revocable Discretionary Approval for use of the site.

Table G.1 Permanent and Operational Source Control Measures

ble G.1 Permanent and Operational Source Control Measures			
Potential Sources of Runoff pollutants	Permanent Structural Source Control BMPs	Operational Source Control BMPs	
Storm drain inlets	Permanent controls – Mark all inlets with the words "Only Rain Down the Storm Drain" or similar. Catch basin Markers may be available from the Riverside County Flood Control and Water Conservative District, call 951.955.1200 to verify.	Maintain and periodically repaint or replace inlet markings. See applicable operational BMPs in Fact Sheet SC-44, "Drainage System Maintenance", in the CASQA Stormwater Quality Handbook at www.cabmphandbooks.com	
Future indoor and structural pest control	Note building design features that discourage entry of pests.	Provide Integrated Pest Management information to owners, lessees, and operators.	
Trash Storage Areas	Permanent Control – State that signs will be provided on or near dumpsters with the words "Do	Provide adequate number of receptacles. Inspect receptacles regularly, repair or replace leaky receptacles. Keep receptacles	

Diago, Sidowalko and	not dump hazardous materials here" or similar	covered. Prohibit/prevent dumping of liquid or hazardous wastes. Post "no hazardous materials" signs. Inspect and pick up litter daily and clean up spills immediately. Keep spill control materials available on-site. See Fact Sheet SC-34, "Waste Handling and Disposal" in the CASQA Stormwater Quality Handbooks at www.cabmphandbooks.com
Plazas, Sidewalks and Parking Lots		Sweep plazas, sidewalks, and parking lots regularly to prevent accumulation of litter and debris. Collect debris from pressure washing to prevent entry into storm drain system. Collect washwater containing any cleaning agent or degreaser and discharge to the sanitary sewer not to a storm drain.
Landscape / Outdoor Pesticide Use	Design landscaping to minimize irrigation and runoff, to promote surface infiltration where appropriate, and to minimize the use of fertilizers and pesticides that contribute to stormwater pollution. Where landscaped areas are used to retain or detain stormwater, specify plants that are tolerant of saturated soil conditions.	Maintain landscaping using minimum or no pesticides. See applicable operational BMPs in "What you should know See applicable operational BMPs in "What you should know http://rcflood.org/stormwater/Error! Hyperlink reference not valid. Provide IPM information to new owners, lessees and operators.
Miscellaneous Drain or Wash Water or Other Sources Boiler drain lines Condensate drain lines Roofing, gutters, and trim.	Boiler drain lines shall be directly or indirectly connected to the sanitary sewer system and may not discharge to the storm drain system. Condensate drain lines may discharge to landscaped areas if the flow is small enough that runoff will not occur. Condensate drain lines may not discharge to the storm drain system. Avoid roofing, gutters, and trim made of copper or other unprotected metals that may leach into runoff.	

Section H: Construction Plan Checklist

Populate Table H.1 below to assist the plan checker in an expeditious review of your project. The first two columns will contain information that was prepared in previous steps, while the last column will be populated with the corresponding plan sheets. This table is to be completed with the submittal of your final Project-Specific WQMP.

Table H.1 Construction Plan Cross-reference

BMP No. or ID	BMP Identifier and Description	Corresponding Plan Sheet(s)	BMP Location (Lat/Long)

Note that the updated table — or Construction Plan WQMP Checklist — is **only a reference tool** to facilitate an easy comparison of the construction plans to your Project-Specific WQMP. Co-Permittee staff can advise you regarding the process required to propose changes to the approved Project-Specific WQMP.

Section I: Operation, Maintenance and Funding

The Copermittee will periodically verify that Stormwater BMPs on your site are maintained and continue to operate as designed. To make this possible, your Copermittee will require that you include in Appendix 9 of this Project-Specific WQMP:

- 1. A means to finance and implement facility maintenance in perpetuity, including replacement cost.
- 2. Acceptance of responsibility for maintenance from the time the BMPs are constructed until responsibility for operation and maintenance is legally transferred. A warranty covering a period following construction may also be required.
- 3. An outline of general maintenance requirements for the Stormwater BMPs you have selected.
- 4. Figures delineating and designating pervious and impervious areas, location, and type of Stormwater BMP, and tables of pervious and impervious areas served by each facility. Geolocating the BMPs using a coordinate system of latitude and longitude is recommended to help facilitate a future statewide database system.
- 5. A separate list and location of self-retaining areas or areas addressed by LID Principles that do not require specialized O&M or inspections but will require typical landscape maintenance as noted in Chapter 5, pages 85-86, in the WQMP Guidance. Include a brief description of typical landscape maintenance for these areas.

Your local Co-Permittee will also require that you prepare and submit a detailed Stormwater BMP Operation and Maintenance Plan that sets forth a maintenance schedule for each of the Stormwater BMPs built on your site. An agreement assigning responsibility for maintenance and providing for inspections and certification may also be required.

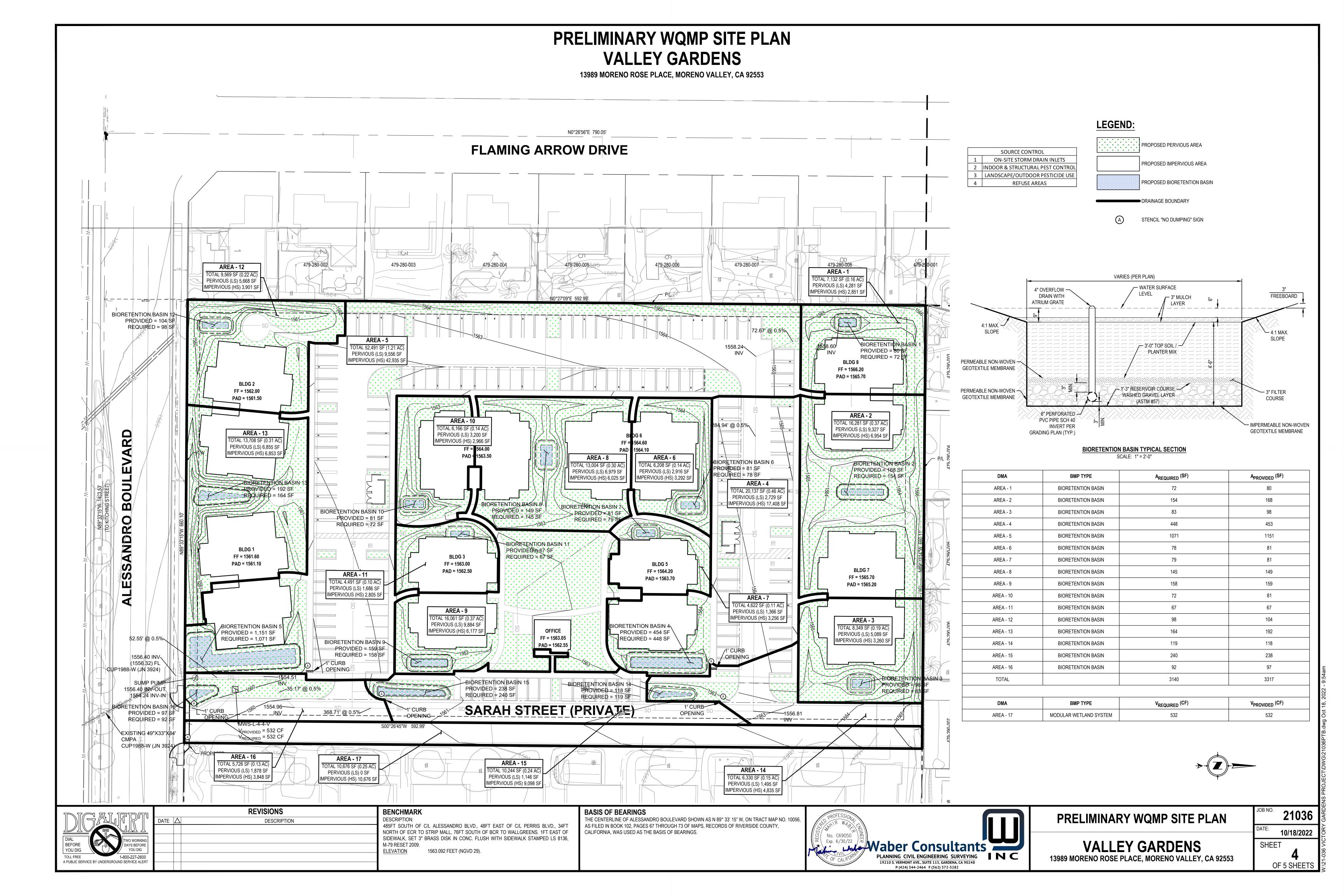
Details of these requirements and instructions for preparing a Stormwater BMP Operation and Maintenance Plan are in Chapter 5 of the WQMP Guidance Document.

Maintenance Mechanism:	Owner shall perform maintenance when there is standing water for more than 72 hours and trash and debris accumulation. The owner pays the qualified contractor to perform required maintenance.
Will the proposed BMPs be massociation (POA)?	naintained by a Home Owners' Association (HOA) or Property Owners
☐ Y	

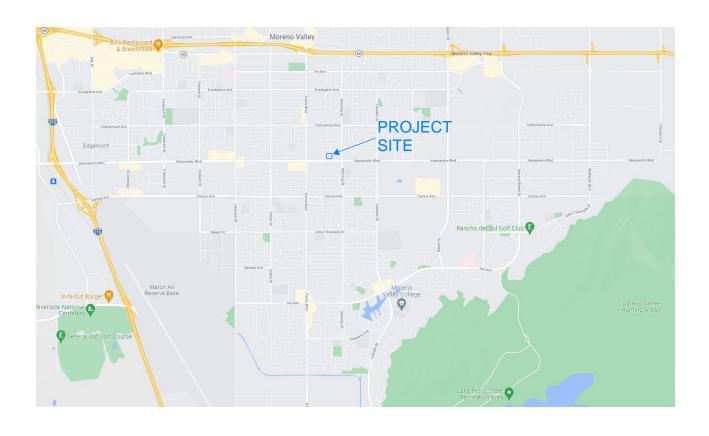
Include your Operation and Maintenance Plan and Maintenance Mechanism in Appendix 9. Additionally, include all pertinent forms of educational materials for those personnel that will be maintaining the proposed BMPs within this Project-Specific WQMP in Appendix 10.

Appendix 1: Maps and Site Plans

Location Map, WQMP Site Plan and Receiving Waters Map

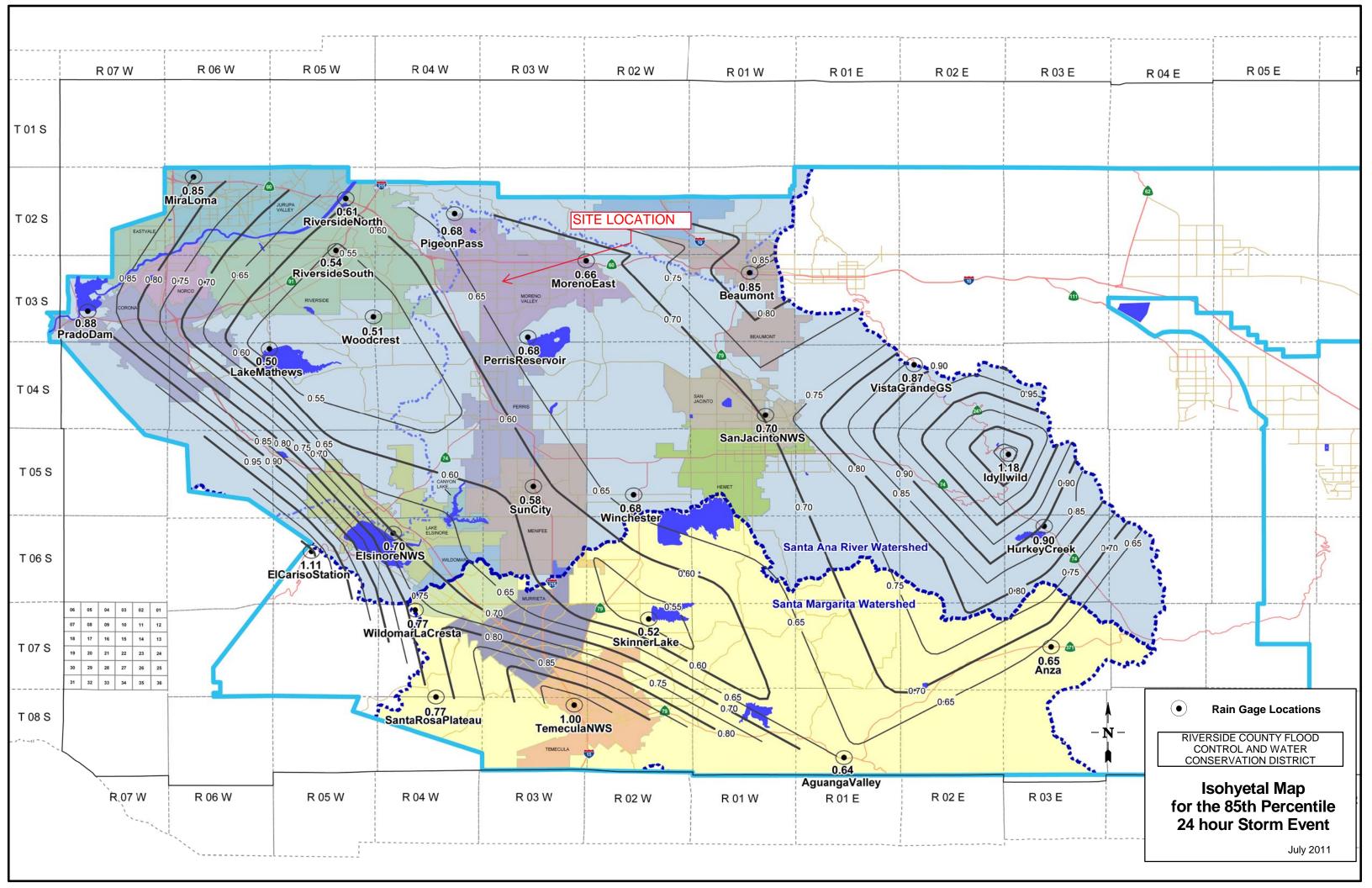


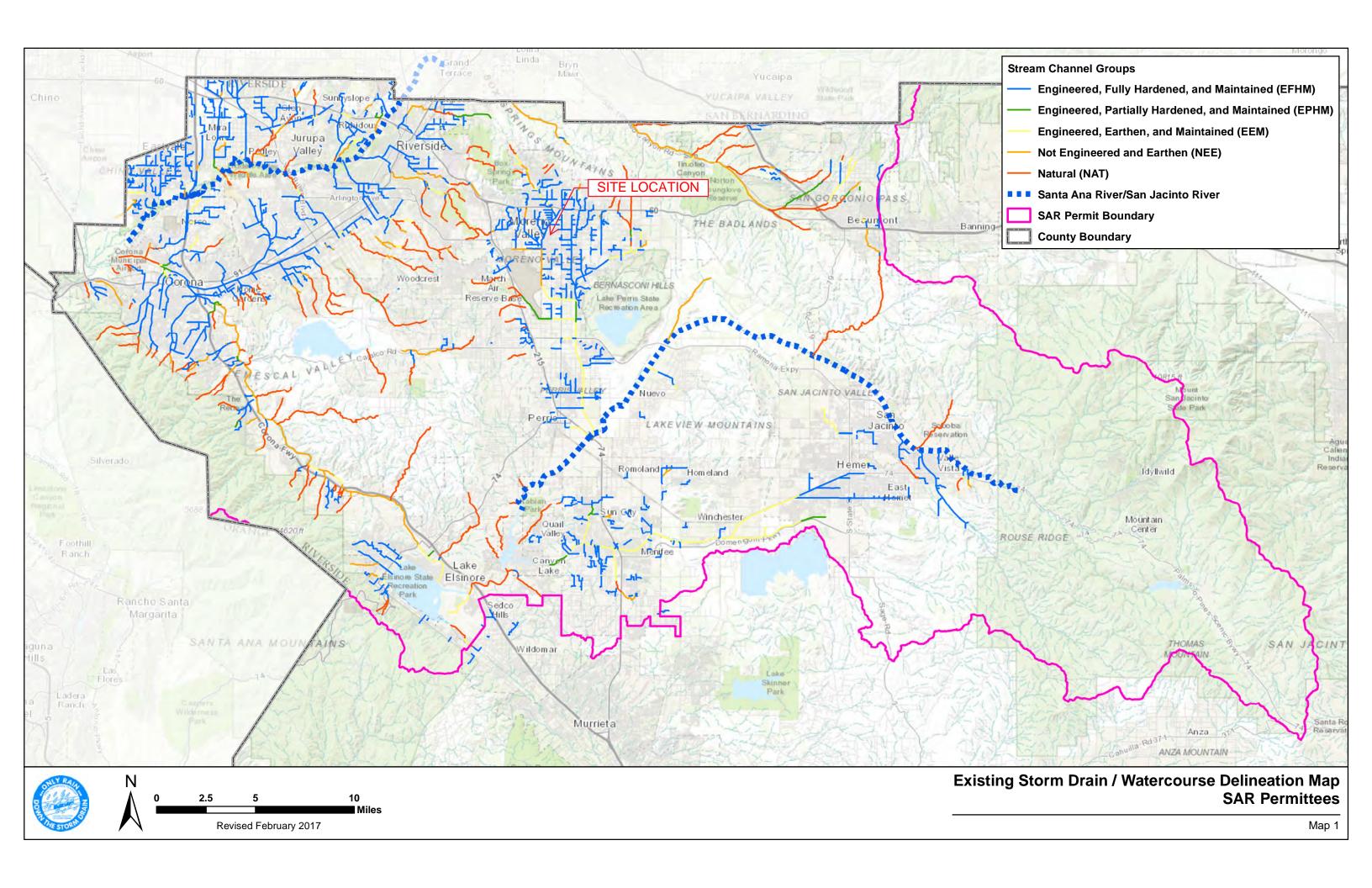
LOCATION MAP



RECEIVING WATER MAPS

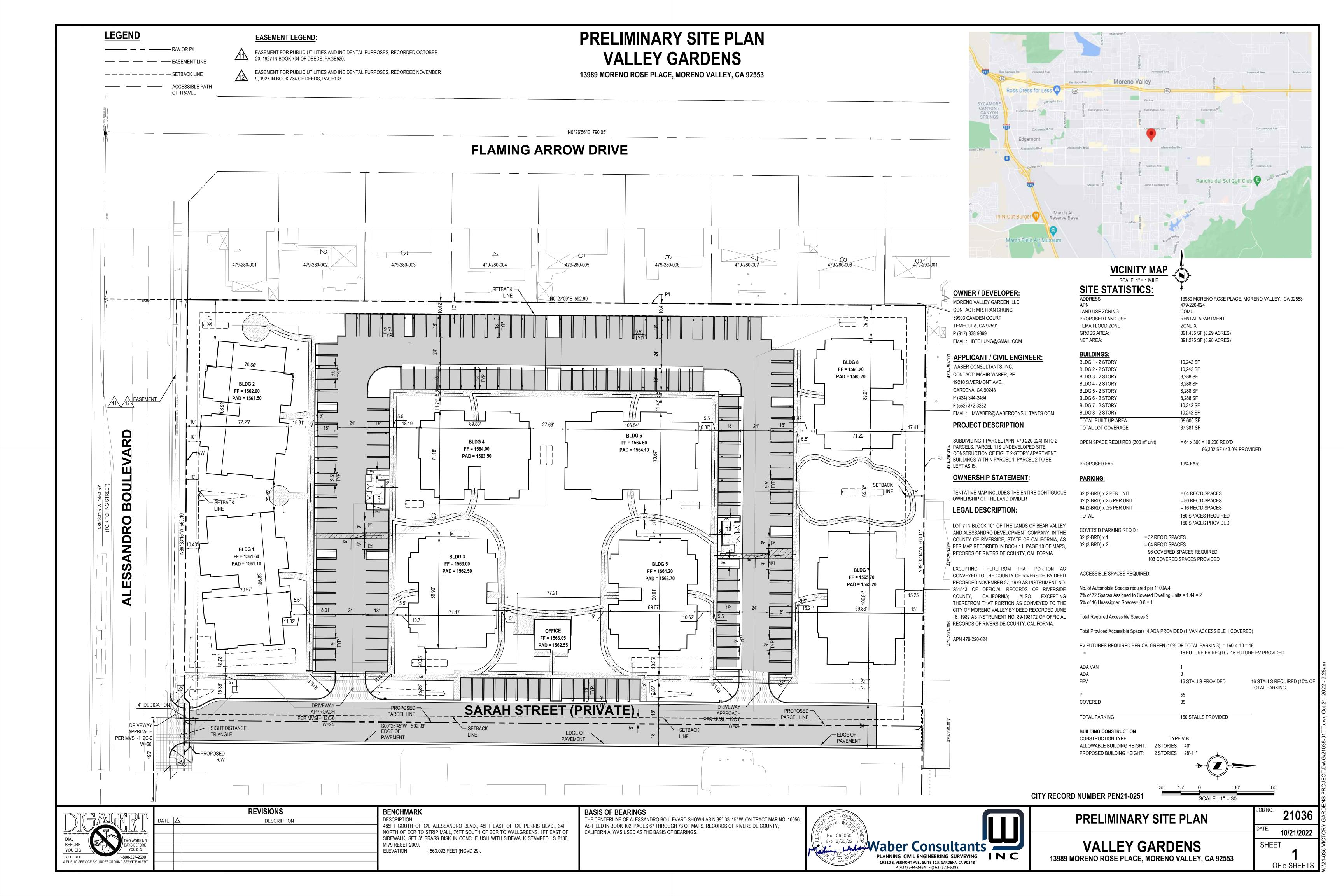






Appendix 2: Construction Plans

Grading and Drainage Plans



PRELIMINARY GRADING PLAN **VALLEY GARDENS**

13989 MORENO ROSE PLACE, MORENO VALLEY, CA 92553

OWNER / DEVELOPER: MORENO VALLEY GARDEN, LLC CONTACT: MR.TRAN CHUNG 39903 CAMDEN COURT TEMECULA, CA 92591 P (917)-838-9869 EMAIL: IBTCHUNG@GMAIL.COM

APPLICANT / CIVIL ENGINEER:

WABER CONSULTANTS, INC. CONTACT: MAHIR WABER, PE. 19210 S.VERMONT AVE., GARDENA, CA 90248 P (424) 344-2464 F (562) 372-3282

EMAIL: MWABER@WABERCONSULTANTS.COM

PROJECT DESCRIPTION

SUBDIVIDING 1 PARCEL (APN: 479-220-024) INTO 2 PARCELS. PARCEL 1 IS UNDEVELOPED SITE. CONSTRUCTION OF EIGHT 2-STORY APARTMENT BUILDINGS WITHIN PARCEL 1. PARCEL 2 TO BE LEFT AS IS.

OWNERSHIP STATEMENT:

TENTATIVE MAP INCLUDES THE ENTIRE CONTIGUOUS OWNERSHIP OF THE LAND DIVIDER

LEGAL DESCRIPTION:

LOT 7 IN BLOCK 101 OF THE LANDS OF BEAR VALLEY AND ALESSANDRO DEVELOPMENT COMPANY, IN THE COUNTY OF RIVERSIDE, STATE OF CALIFORNIA, AS PER MAP RECORDED IN BOOK 11, PAGE 10 OF MAPS, RECORDS OF RIVERSIDE COUNTY, CALIFORNIA.

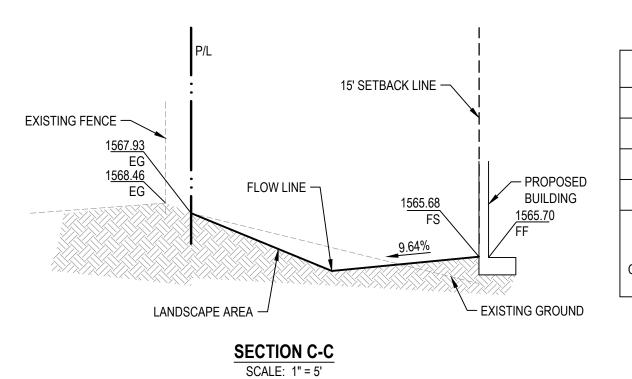
EXCEPTING THEREFROM THAT PORTION AS CONVEYED TO THE COUNTY OF RIVERSIDE BY DEED RECORDED NOVEMBER 27, 1979 AS INSTRUMENT NO. 251543 OF OFFICIAL RECORDS OF RIVERSIDE COUNTY, CALIFORNIA; ALSO EXCEPTING THEREFROM THAT PORTION AS CONVEYED TO THE CITY OF MORENO VALLEY BY DEED RECORDED JUNE 16, 1989 AS INSTRUMENT NO. 89-198172 OF OFFICIAL RECORDS OF RIVERSIDE COUNTY, CALIFORNIA.

APN 479-220-024

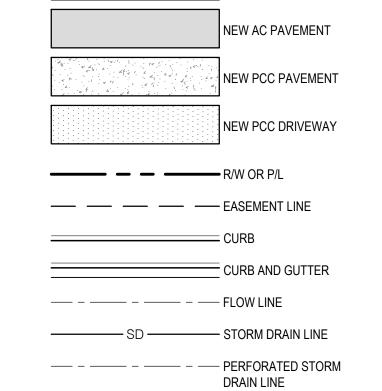
TOPOGRAPHY

TOPOGRAPHICAL SURVEY WAS PERFORMED ON AUGUST 17TH, 2021 BY WABER CONSULTANTS, INC.

<u>UTILITY COMPANIES</u>	EMERGENCY NUMI
BOX SPRINGS MUTUAL WATER COMPANY	(951) 653-6419
CHARTER SPECTRUM	(877) 906-9121
EASTERN MUNICIPAL WATER DIST	(951) 928-3777
EDGEMONT COMMUNITY SERVICES DISTRICT	(951) 784-2632
FRONTIER COMMUNICATION	(800) 921-8101
SC EDISON COMPANY	(800) 655-4555
SC GAS COMPANY	(800) 427-2200
SUNESYS	(951) 278-0400
RIVERSIDE TRANSIT AGENCY	(951) 565-5164
UNDERGROUND SERVICE ALERT	(800) 227-2600
MORENO VALLEY UTILITY ADMINISTRATION	(951) 413-3500
SPECIAL DISTRICTS ADMINISTRATION	(951) 413-3480
TRAFFIC SIGNAL MAINTENANCE (CITY)	(951) 413-3140
VERIZON WIRELESS	(800) 922-0204



LEGEND:



NEW PCC SIDEWALK

ABBREVIATIONS:

ASPHALT CONCRETE **CURB FACE EXISTING** FINISHED FLOOR FLOW LINE MAXIMUM MINIMUM PROPERTY LINE PCC PORTLAND CEMENT CONCRETE R/W RIGHT OF WAY RIDGE LINE

SITE STATISTICS:

ADDRESS 13989 MORENO ROSE PLACE, MORENO VALLEY, CA 92553 479-220-024 COMU LAND USE ZONING PROPOSED LAND USE RENTAL APARTMENT FEMA FLOOD ZONE ZONE X GROSS AREA: 391,435 SF (8.99 ACRES) NET AREA: 391.275 SF (8.98 ACRES)

PARCEL: 1 200,519 SQ. FT. (4.60 AC)

BLDG 1 - 2 STORY BLDG 2 - 2 STORY

10,242 SF 10,242 SF BLDG 3 - 2 STORY 8,288 SF BLDG 4 - 2 STORY 8,288 SF BLDG 5 - 2 STORY 8,288 SF 8,288 SF BLDG 6 - 2 STORY BLDG 7 - 2 STORY 10,242 SF BLDG 8 - 2 STORY 10,242 SF

69,600 SF TOTAL BUILT UP AREA TOTAL LOT COVERAGE 37,381 SF

OPEN SPACE REQUIRED (300 sf/ unit) = 64 x 300 = 19,200 REQ'D 86,302 SF / 43.9% PROVIDED

PROPOSED FAR 19% FAR

BUILDING CONSTRUCTION

CONSTRUCTION TYPE: TYPE V-B ALLOWABLE BUILDING HEIGHT: 2 STORIES 40' PROPOSED BUILDING HEIGHT: 2 STORIES 28'-11"

PARCEL: 2 190,916 SQ. FT. (4.38 AC)

EXISTING RESIDENCE HOMES

ESTIMATED EARTHWORK QUANTITIES				
CUT 1,112 CY				
FILL 7,626 CY				
IMPORT 6,514 CY				
EXPORT -				
EARTHWORK QUANTITIES SHOWN ARE RAW ESTIMATES ONLY INTENDED FOR ESTABLISHING				

CONTRACTOR SHALL BE RESPONSIBLE FOR DETERMINING THE QUANTITIES FOR BID PURPOSES AND ANY EXPORT OR IMPORT REQUIRED TO BALANCE THE SITE.

I		C/L 127'				
•	60'		67'			
5'	45.79'	18.17'	46.26'	~1.	6.79'	5'
EX. C & GU	CURB EX. AC — UTTER PAVEMENT ===================================	RAISED MEDIAN	EX. AC PAVEMENT	EX. CURB — & GUTTER	-y==	==
EX. SIDEWALK		TYPICAL SECTION ALESSANDRO BOULEVARD		EX. LANDSCAPE	E) SIDEWALI	
		DIVIDED MAJOR ARTERIAL				
		STD DWG MVSI-101A-0				

SCALE: 1" = 10'

- 10' SETBACK LINE EXISTING FENCE -/ 1564.47 /FS PCC /— EXISTING GROUND PAVEMENT 6" CONC. -

SECTION B-B

REVISIONS DESCRIPTION YOU DIG

A PUBLIC SERVICE BY UNDERGROUND SERVICE ALERT

BENCHMARK

DESCRIPTION: 485FT SOUTH OF C/L ALESSANDRO BLVD., 48FT EAST OF C/L PERRIS BLVD., 34FT NORTH OF ECR TO STRIP MALL, 76FT SOUTH OF BCR TO WALLGREENS. 1FT EAST OF SIDEWALK, SET 3" BRASS DISK IN CONC. FLUSH WITH SIDEWALK STAMPED LS 8136, 1563.092 FEET (NGVD 29).

BASIS OF BEARINGS

THE CENTERLINE OF ALESSANDRO BOULEVARD SHOWN AS N 89° 33' 15" W, ON TRACT MAP NO. 10056, AS FILED IN BOOK 102, PAGES 67 THROUGH 73 OF MAPS, RECORDS OF RIVERSIDE COUNTY, CALIFORNIA, WAS USED AS THE BASIS OF BEARINGS.



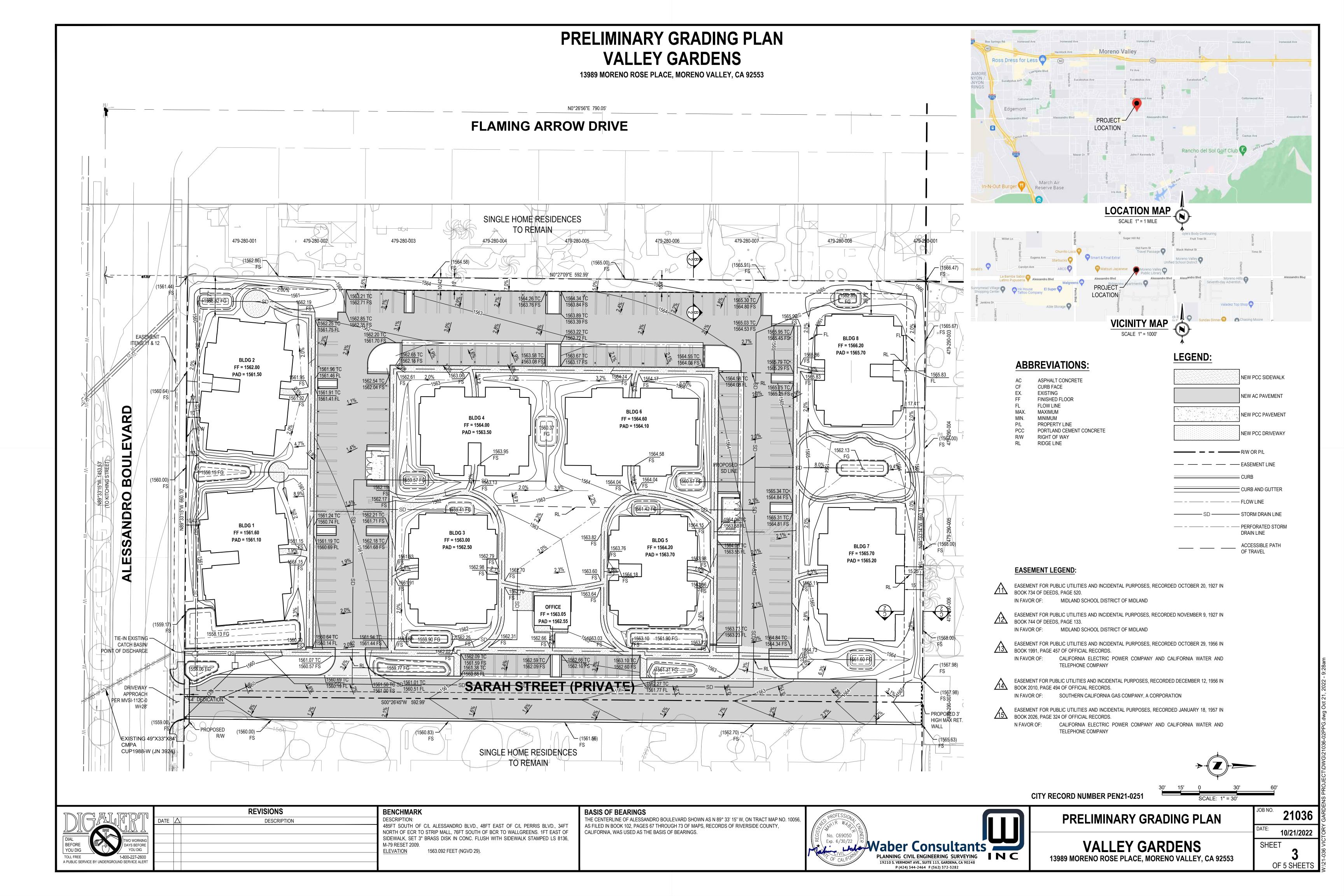
CITY RECORD NUMBER PEN21-0251

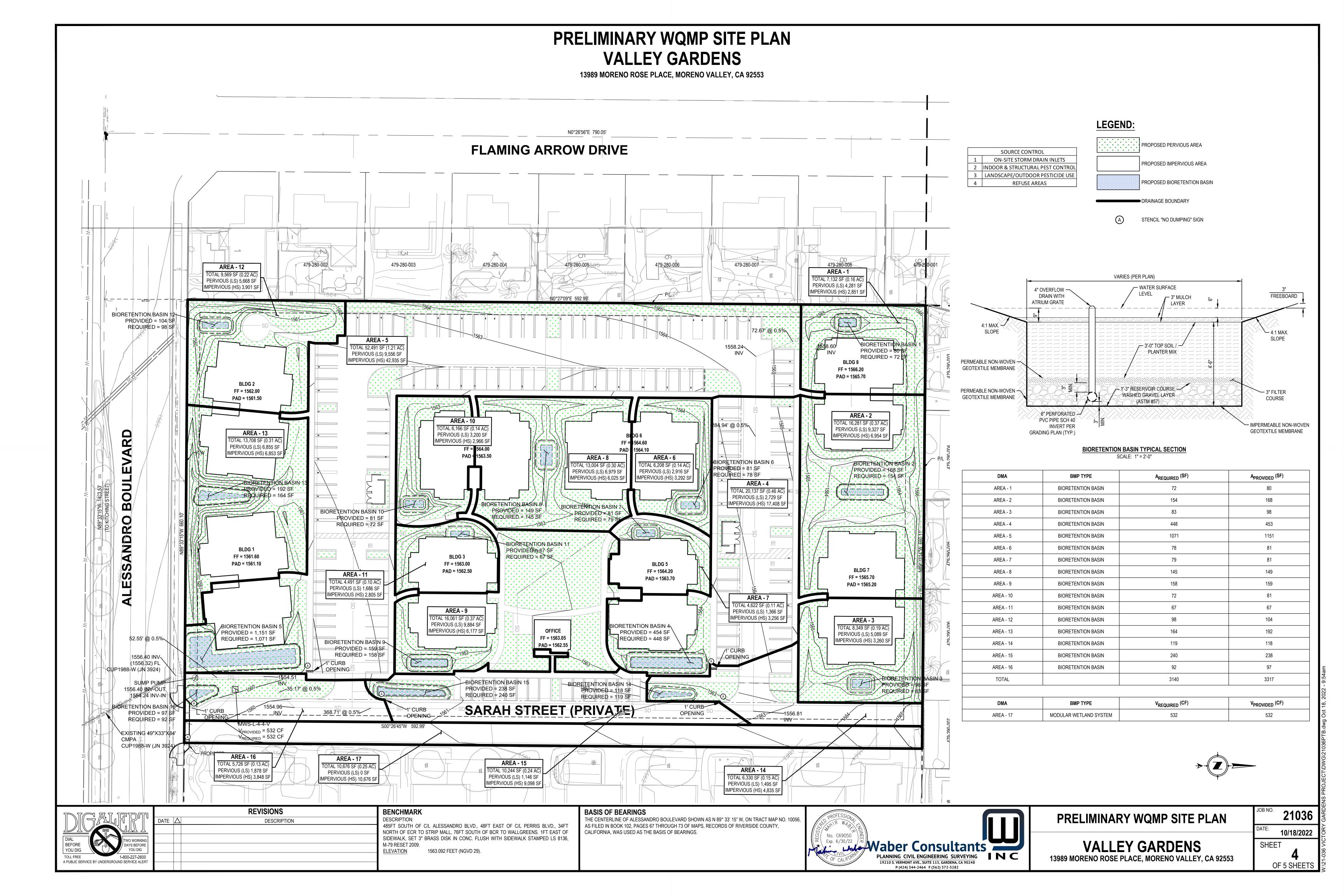
PRELIMINARY GRADING PLAN

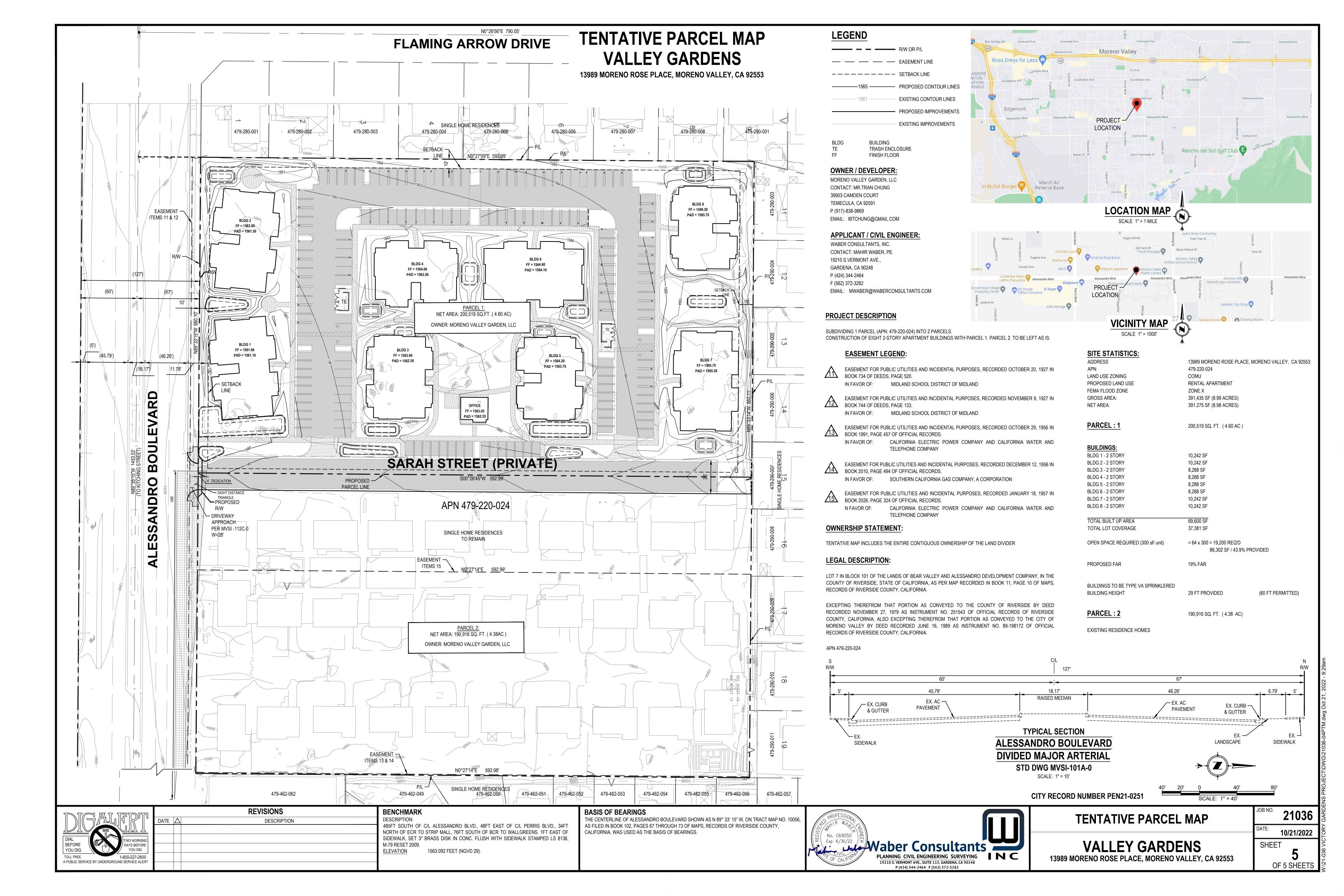
VALLEY GARDENS 13989 MORENO ROSE PLACE, MORENO VALLEY, CA 92553

JOB NO.	21036
DATE:	10/21/2022
<u> </u>	_

SHEET OF 5 SHEETS







Appendix 3: Soils Information

Geotechnical Study and Other Infiltration Testing Data

Geotechnical Engineering Investigation Proposed Multi-Unit Residential Development North of Alessandro Boulevard and East of Flaming Arrow Drive City of Moreno Valley, California

Tran Chung 39903 Camden Court Temecula, California 92591

Project Number 22686-21 August 27, 2021

NorCal Engineering

Soils and Geotechnical Consultants 10641 Humbolt Street Los Alamitos, CA 90720 (562) 799-9469 Fax (562) 799-9459

August 27, 2021

Project Number 22686-21

Tran Chung 39903 Camden Court Temecula, California 92591

RE: Geotechnical Engineering Investigation - Proposed Multi-Unit Residential Development - Located North of Alessandro Boulevard and East of Flaming Arrow Drive, in the City of Moreno Valley, California

Dear Mr. Chung:

Pursuant to your request, this firm has performed a Geotechnical Engineering Investigation for the above referenced project in accordance with your approval of our proposal dated July 13, 2021. The purpose of this investigation is to evaluate the geotechnical conditions of the subject site and to provide recommendations for the proposed multi-unit residential development.

The scope of work included the following: 1) site reconnaissance; 2) subsurface geotechnical exploration and sampling; 3) laboratory testing; 4) soil infiltration testing; 5) engineering analysis of field and laboratory data; 5) preparation of a geotechnical engineering report. It is the opinion of this firm that the proposed development is feasible from a geotechnical standpoint provided that the recommendations presented in this report are followed in the design and construction of the project.

1.0 Project Description

It is proposed to construct a two-story, 67-unit residential development as shown on the attached Site Plan by Irwin Partners Architects dated August, 5 2021. Other improvements will include asphalt and/or concrete driveways, hardscape and landscaping. The proposed grading will consist of cuts on the order of a few feet with minor fills to achieve finished grade elevations. Final building plans shall be reviewed by this firm prior to submittal for city approval to determine the need for any additional study and revised recommendations pertinent to the proposed development, if necessary.

2.0 Site Description

The subject property is located along the north side of Alessandro Boulevard, east of Flaming Arrow Drive, in the City of Moreno Valley. The generally rectangular shaped parcel is elongated in a north to south direction. The site is relatively level with topography descending gradually from north to south on the order of a few feet. The site is currently vacant and covered in light vegetation.

3.0 Site Exploration

The field investigation consisted of the placement of ten (10) subsurface exploratory trenches by a backhoe to depths ranging between 5 and 16 feet below current ground elevations. The explorations were visually classified and logged by a field engineer with location of the subsurface explorations shown on the attached Site Plan. The exploratory borings revealed the existing earth materials to consist of fill and natural soil. Detailed descriptions of the subsurface conditions are listed on the boring logs in Appendix A. It should be noted that the transition from one soil type to another as shown on the borings logs is approximate and may in fact be a gradual transition. The soils encountered are described as follows:

Fill: A fill soil classifying as a brown, clayey SILT with some sand and occasional gravel, concrete and rootlets was encountered across the site to a depth of 1 to 1½ feet below ground surface. These soils were noted to be soft to medium stiff and dry.

Natural: An undisturbed native soil classifying as brown, silty sandy CLAY was encountered beneath the fill soils. The native soils were observed to be medium stiff to stiff and dry to damp.

The overall engineering characteristics of the earth material were relatively uniform with each excavation. No groundwater was encountered to the depths of our borings and no caving occurred.

4.0 Laboratory Tests

Relatively undisturbed samples of the subsurface soils were obtained to perform laboratory testing and analysis for direct shear, consolidation tests, and to determine in-place moisture/densities. These relatively undisturbed ring samples were obtained by driving a thin-walled steel sampler lined with one-inch-long brass rings with an inside diameter of 2.42 inches into the undisturbed soils. The sampler was driven a total of six inches into undisturbed soils. Bulk bag samples were obtained in the upper soils for expansion index tests and maximum density tests. All test results are included in Appendix B, unless otherwise noted.

- 4.1 **Field Moisture Content** (ASTM: D 2216) and the dry density of the ring samples were determined in the laboratory. This data is listed on the logs of explorations.
- 4.2 **Maximum Density tests** (ASTM: D 1557) were performed on typical samples of the upper soils. Results of these tests are shown on Table I.
- 4.3 **Expansion Index tests** (ASTM: D 4829) were performed on remolded samples of the upper soils to determine expansive characteristics. Results of these tests are provided on Table II.
- 4.4 **Atterberg Limits** (ASTM: D 4318) consisting of liquid limit, plastic limit and plasticity index were performed on representative soil samples. Results are shown on Table III.
- 4.5 **Corrosion tests** consisting of sulfate, pH, resistivity and chloride analysis to determine potential corrosive effects of soils on concrete and underground utilities. Test results are provided on Table IV.
- 4.6 **R-Value test** per California Test Method 301 was performed on a representative sample, which may be anticipated to be near subgrade to determine pavement design. Results are provided within the pavement design section of the report.

- 4.7 **Direct Shear tests** (ASTM: D 3080) were performed on undisturbed and/or remolded samples of the subsurface soils. The test is performed under saturated conditions at loads of 1,000 lbs./sq.ft., 2,000 lbs./sq.ft., and 3,000 lbs./sq.ft. with results shown on Plate A.
- 4.8 **Consolidation tests** (ASTM: D 2435) were performed on undisturbed samples to determine the differential and total settlement which may be anticipated based upon the proposed loads. Water was added to the samples at a surcharge of one KSF and the settlement curves are plotted on Plates B and C.

5.0 Seismicity Evaluation

The proposed development lies outside of any Alquist-Priolo Special Studies Zone and the potential for damage due to direct fault rupture is considered unlikely. The San Jacinto (Valley Segment) Fault is located approximately 7 kilometers from the site and is capable of producing a Magnitude 6.9 earthquake. Ground shaking originating from earthquakes along other active faults in the region is expected to induce lower horizontal accelerations due to smaller anticipated earthquakes and/or greater distances to other faults. The seismic design acceleration parameters are provided below and are based on the 2019 California Building Code (CBC) for the referenced project. The data was obtained from the American Society of Civil Engineers (ASCE) website, https://asce7hazardtool.online/ and is attached in Appendix C.

Seismic Design Acceleration Parameters

Latitude	33.918
Longitude	-117.221
Site Class	D
Risk Category	
Mapped Spectral Response Acceleration	S _S = 1.653
	$S_1 = 0.644$
Adjusted Maximum Acceleration	S _{MS} = 1.653
Design Spectral Response Acceleration Parameters	S _{DS} = 1.102
Peak Ground Acceleration	$PGA_{M} = 0.77$

Use of these values is dependent on requirements of ASCE 7-16, 11-4.8, Exception 2 that requires the value of the seismic response coefficient C_s be determined by Equation 12.8.2 for values of $T \le 1.5T_s$ and taken as equal to 1.5 times the value computed in accordance with either 12.8-3 for $T_L \ge T \ge 1.5T_s$ or Equation 12.8-4 for $T > T_L$. Computations and verification of these conditions is referred to the structural engineer.

6.0 <u>Liquefaction Evaluation</u>

The site is expected to experience ground shaking and earthquake activity that is typical of the Southern California area. It is during severe shaking that loose, granular soils below the groundwater table can liquefy. Based on review of the *City of Moreno Valley Geological Faults and Liquefaction Map (September 22, 2016, revised May 2017)*, the site is <u>not</u> situated in an area of generalized liquefaction susceptibility. Thus, design of the proposed construction in conformance with the latest Building Code provisions for earthquake design is expected to provide mitigation of ground shaking hazards that are typical in Southern California.

7.0 Infiltration Characteristics

Infiltration tests within the site were performed to provide preliminary infiltration rates for the purpose of planning and design of an on-site water disposal system. The infiltration tests consisted of the double ring infiltration test per ASTM Method D 3385. The field infiltration rate was computed using a reduction factor – Rf based on the field measurements with our calculations given in Appendix D. Based upon the results of our testing, the soils encountered in the planned on-site drainage disposal system area exhibit the following infiltration rates.

Boring/Test No.	Depth	Soil Classification	Field Infiltration Rate	Design Rate
T-1	5'	Silty Sandy CLAY	0.58 in/hr	0.19 in/hr
T-2	7.5'	Silty SAND	0.64 in/hr	0.21 in/hr

Based on the results of our field testing, the subsurface soils encountered in the proposed onsite drainage disposal system shall utilize the design infiltration rates based on a safety factor of 3.0 or greater in compliance with the County of Riverside "Low Impact Development BMP Design" guidelines. All systems must meet the latest city and/or county specifications and the California Regional Water Quality Control Board (CRWQCB) requirements.

The infiltration rates at the depths tested indicate the stiff/dense soils encountered in our test locations <u>are not</u> suitable for storm water infiltration at the project site. The recommendations and conclusions contained in this report are based upon the soil conditions encountered in the test excavations.

8.0 Conclusions and Recommendations

Based upon our evaluations, the proposed development is acceptable from a geotechnical engineering standpoint. By following the recommendations and guidelines set forth in our report, the structures will be safe from excessive settlements under the anticipated design loadings and conditions. The proposed development shall meet all requirements of the City Building Ordinance and will not impose any adverse effect on existing adjacent structures.

The following recommendations are based upon soil conditions encountered in our field investigation; these near-surface soil conditions could vary across the site. Variations in the soil conditions may not become evident until the commencement of grading operations for the proposed development and revised recommendations from the soils engineer may be necessary based upon the conditions encountered.

It is recommended that site inspections are performed by a representative of this firm during all grading and construction of the development to verify the findings and recommendations documented in this report. The following sections present a discussion of geotechnical related requirements for specific design recommendations of different aspects of the project.

8.1 Site Grading Recommendations

All vegetation and demolition debris shall be removed and hauled prior to the start of grading operations. Existing vegetation shall not be mixed or disced into the soils. Any removed soils may be reutilized as compacted fill once any deleterious material or oversized materials (in excess of eight inches) is removed. Grading operations shall be performed in accordance with the attached "Specifications for Compacted Fill Operations".

8.1.1 Removal and Recompaction Recommendations

All disturbed soils and/or fill (about 1 to 1½ feet below ground surface) shall be removed to competent native material, the exposed surface scarified to a depth of 12 inches, brought to within 2% of optimum moisture content and compacted to a minimum of 90% of the laboratory standard (ASTM: D 1557) prior to placement of any additional compacted fill soils, foundations, slabs-on-grade and pavement. Grading shall extend a minimum of five horizontal feet outside the edges of foundations or equidistant to the depth of fill placed, whichever is greater.

It is possible that isolated areas of undiscovered fill not described in this report are present on site; if found, these areas should be treated as discussed earlier. A diligent search shall also be conducted during grading operations in an effort to uncover any underground structures, irrigation or utility lines. If encountered, these structures and lines shall be either removed or properly abandoned prior to the proposed construction.

Any imported fill material should be preferably soil similar to the upper soils encountered at the subject site. All soils shall be approved by this firm prior to importing at the site and will be subjected to additional laboratory testing to assure concurrence with the recommendations stated in this report.

If placement of slabs-on-grade and pavement is not completed immediately upon completion of grading operations, additional testing and grading of the areas may be necessary prior to continuation of construction operations. Likewise, if adverse weather conditions occur which may damage the subgrade soils, additional assessment by the soils engineer as to the suitability of the supporting soils may be needed.

Care should be taken to provide or maintain adequate lateral support for all adjacent improvements and structures at all times during the grading operations and construction phase. Adequate drainage away from the structures, pavement and slopes should be provided at all times.

8.1.2 Fill Blanket Recommendations

Due to the potential for differential settlement of foundations placed on compacted fill and medium stiff native materials, it is recommended that all foundations be underlain by a uniform compacted fill blanket at least two feet in thickness. This fill blanket shall extend a minimum of five horizontal feet outside the edges of foundations or equidistant to the depth of fill placed, whichever is greater.

8.2 Temporary Excavations

Temporary <u>unsurcharged</u> excavations in the existing site materials may be made at vertical inclinations up to 4 feet in height unless cohesionless soils are encountered. In areas where soils with little or no binder are encountered, where adverse geological conditions are exposed, or where excavations are adjacent to existing structures, shoring or flatter excavations may be required. The temporary cut slope gradients given above do not preclude local raveling and sloughing. Once finalized sections are made available, this firm shall review and provide stability calculations with updated excavation recommendations.

Temporary shoring design may utilize an active earth pressure of 25 pcf without any surcharge due to adjacent traffic, equipment or structures. The passive fluid pressures of 250 pcf may be doubled to 500 pcf for temporary design. Any drilled caissons will require to be cased due to the potential of caving. Shoring members should not be vibrated or driven due to the potential for damage to nearby improvements. All excavations shall be made in accordance with the requirements of the geotechnical engineer, CAL-OSHA and other public agencies having jurisdiction. Care should be taken to provide or maintain adequate lateral support for all adjacent improvements and structures at all times during the grading operations and construction phase.

8.3 Foundation Design

All foundations may be designed utilizing an allowable bearing capacity of 2,000 psf for a minimum embedded depth of 24 inches into approved engineered fill. The bearing value may be increased by 500 psf for each additional foot of depth in excess of the 24-inch minimum depth, up to 3,000 psf. A one-third increase may be used when considering short-term loading and seismic forces. All foundations shall be reinforced a minimum of one No. 4 bar, top and bottom. A representative of this firm shall inspect all foundation excavations prior to pouring concrete.

8.4 Settlement Analysis

Resultant pressure curves for the consolidation tests are shown on Plates B and C. Computations utilizing these curves and the recommended allowable soil bearing capacities reveal that the foundations will experience settlements on the order of $\frac{3}{4}$ inch and differential settlements of less than $\frac{1}{4}$ inch.

8.5 Lateral Resistance

The following values may be utilized in resisting lateral loads imposed on the structure. Requirements of the California Building Code should be adhered to when the coefficient of friction and passive pressures are combined.

Coefficient of Friction - 0.35

Equivalent Passive Fluid Pressure = 200 lbs./cu.ft.

Maximum Passive Pressure = 2,000 lbs./cu.ft.

The passive pressure recommendations are valid only for approved compacted fill soils or competent native materials.

8.6 Retaining Wall Design Parameters

Active earth pressures against retaining walls will be equal to the pressures developed by the following fluid densities. These values are for **granular backfill material** placed behind the walls at various ground slopes above the walls.

Surface Slope of Retained Materials (Horizontal to Vertical	Equivalent Fluid Density (lb./cu.ft.)
Level	30
5 to 1	35
4 to 1	38
3 to 1	40
2 to 1	45

Any applicable short-term construction surcharges and seismic forces should be added to the above lateral pressure values. An equivalent fluid pressure of 45 pcf may be utilized for the restrained wall condition with a level grade behind the wall.

The seismic-induced lateral soil pressure for walls greater than 6 feet may be computed using a triangular pressure distribution with the maximum value at the top of the wall. The maximum lateral pressure of (20 pcf) H where H is the height of the retained soils above the wall footing should be used in final design of retaining walls. Sliding resistance values and passive fluid pressure values may be increased by 1/3 during short-term wind and seismic loading conditions.

All walls shall be waterproofed as needed and protected from hydrostatic pressure by a reliable permanent subdrain system. The subsurface drainage system shall consist of a 4-inch diameter perforated PVC pipe encased with gravel and wrapped with filter fabric. The granular backfill to be utilized immediately adjacent to retaining walls shall consist of an approved granular soil with a sand equivalency greater than 30. This backfill zone of free draining material shall consist of a wedge beginning a minimum of one horizontal foot from the base of the wall extending upward at an inclination of no less than ¾ to 1 (horizontal to vertical).

8.7 Slab Design

All slabs shall be a minimum of four inches in thickness reinforced a minimum of No. 3 bars, sixteen inches in each direction and placed on approved subgrade soils. The subgrade soils shall be moisture conditioned 3% over optimum moisture levels in the upper eighteen inches. All concrete slabs for hardscape and driveway areas situated near existing street levels shall be a minimum of four inches in thickness and placed on approved subgrade soils. The subgrade soils shall be moisture conditioned over optimum moisture levels in the upper foot.

A vapor retarder should be utilized in areas which would be sensitive to the infiltration of moisture. This retarder shall meet requirements of ASTM E 96, Water Vapor Transmission of Materials and ASTM E 1745, Standard Specification for Water Vapor Retarders used in Contact with Soil or Granular Fill Under Concrete Slabs. The vapor retarder shall be installed in accordance with procedures stated in ASTM E 1643, Standard practice for Installation of Water Vapor Retarders used in Contact with Earth or Granular Fill Under Concrete Slabs.

The moisture retarder may be placed directly upon compacted subgrade soils conditioned to near optimum moisture levels, although one to two inches of sand beneath the membrane is desirable. The subgrade upon which the retarder is placed shall be smooth and free of rocks, gravel or other protrusions which may damage the retarder. Use of sand above the retarder is under the purview of the structural engineer; if sand is used over the retarder, it should be placed in a dry condition.

8.8 Pavement Section Design

The table below provides a preliminary pavement design based upon a R-Value of 33 for the subgrade soils for the proposed pavement areas. Final pavement design may need to be based on R-Value testing of the subgrade soils near the conclusion of site grading to assure that these soils are consistent with those assumed in this preliminary design.

Type of Traffic	Traffic Index	Asphalt (in.)	Base Material (in.)
Automobile Parking Stalls	4.0	3.0	4.0
Light Vehicle Traffic Areas	5.5	3.5	6.5

Any concrete slab-on-grade in pavement areas shall be a minimum of six inches in thickness reinforced and placed on approved subgrade soils. All pavement areas shall have positive drainage toward an approved outlet from the site. Drain lines behind curbs and/or adjacent to landscape areas should be considered by client and the appropriate design engineers to prevent water from infiltrating beneath pavement. If such infiltration occurs, damage to pavement, curbs and flow lines, especially on sites with expansive soils, may occur during the life of the project.

Any approved base material shall consist of a Class II aggregate or equivalent and should be compacted to a minimum of 95% relative compaction. All pavement materials shall conform to the requirements set forth by the City of Riverside. The base material; and asphaltic concrete should be tested prior to delivery to the site and during placement to determine conformance with the project specifications. A pavement engineer shall designate the specific asphalt mix design to meet the required project specifications.

8.9 Utility Trench and Excavation Backfill

Trenches from installation of utility lines and other excavations may be backfilled with on-site soils or approved imported soils compacted to a minimum of 90% relative compaction. All utility lines shall be properly bedded with clean sand having a sand equivalency rating of 30 or more. This bedding material shall be thoroughly water jetted around the pipe structure prior to placement of compacted backfill soils.

8.10 Corrosion Design Criteria

Representative samples of the surficial soils, typical of the subgrade soils expected to be encountered within foundation excavations and underground utilities were tested for corrosion potential. The minimum resistivity value obtained for the samples tested is representative of an environment that may be severely corrosive to metals. The soil pH value was considered to be neutral and may not have a significant effect on soil corrosivity.

Consideration should be given to corrosion protection systems for buried metal such as protective coatings, wrappings or the use of PVC where permitted by local building codes. According to Table 4.3.1 of ACI 318 Building Code and Commentary, these contents revealed negligible sulfate concentrations. Therefore, a Type II cement according to latest CBC specifications may be utilized for building foundations at this time. It is recommended that additional sulfate tests be performed at the completion of site grading to assure that the as graded conditions are consistent with the recommendations stated in this design. Corrosion test results may be found on the attached Table III.

8.11 Expansive Soil

The upper on-site soils are low un expansion potential (El 21-50). When soils have an expansion index (El) of 20 or more, special attention should be given to the project design and maintenance. The attached *Expansive Soil Guidelines* should be reviewed by the engineers, architects, owner, maintenance personnel and other interested parties and considered during the design of the project and future property maintenance. Expansion test results may be found on the attached Table II.

9.0 Closure

The recommendations and conclusions contained in this report are based upon the soil conditions uncovered in our test excavations. No warranty of the soil condition between our excavations is implied. NorCal Engineering should be notified for possible further recommendations if unexpected to unfavorable conditions are encountered during construction phase. It is the responsibility of the owner to ensure that all information within this report is submitted to the Architect and appropriate Engineers for the project.

This firm should have the opportunity to review the final plans (72 hours required) to verify that all our recommendations are incorporated. This report and all conclusions are subject to the review of the controlling authorities for the project.

A preconstruction conference should be held between the developer, general contractor, grading contractor, city inspector, architect, and soil engineer to clarify any questions relating to the grading operations and subsequent construction. Our representative should be present during the grading operations and construction phase to certify that such recommendations are complied within the field.

This geotechnical investigation has been conducted in a manner consistent with the level of care and skill exercised by members of our profession currently practicing under similar conditions in the Southern California area. No other warranty, expressed or implied is made.

We appreciate this opportunity to be of service to you. If you have any further questions, please do not hesitate to contact the undersigned.

Respectfully submitted

NORCAL ENGINEER

Keith D. Tucker Project Engineer

R.G.E. 841

Mike Barone Project Manager

SPECIFICATIONS FOR PLACEMENT OF COMPACTED FILL

Excavation

Any existing low-density soils and/or saturated soils shall be removed to competent natural soil under the inspection of the Geotechnical Engineering Firm. After the exposed surface has been cleansed of debris and/or vegetation, it shall be scarified until it is uniform in consistency, brought to the proper moisture content and compacted to a minimum of 90% relative compaction (in accordance with ASTM: D 1557).

In any area where a transition between fill and native soil or between bedrock and soil are encountered, additional excavation beneath foundations and slabs will be necessary in order to provide uniform support and avoid differential settlement of the structure.

Material for Fill

The on-site soils or approved import soils may be utilized for the compacted fill provided they are free of any deleterious materials and shall not contain any rocks, brick, asphaltic concrete, concrete or other hard materials greater than eight inches in maximum dimensions. Any import soil must be approved by the Geotechnical Engineering firm a minimum of 72 hours prior to importation of site.

Placement of Compacted Fill Soils

The approved fill soils shall be placed in layers not excess of six inches in thickness. Each lift shall be uniform in thickness and thoroughly blended. The fill soils shall be brought to within 2% of the optimum moisture content, unless otherwise specified by the Geotechnical Engineering firm. Each lift shall be compacted to a minimum of 90% relative compaction (in accordance with ASTM: D 1557) and approved prior to the placement of the next layer of soil. Compaction tests shall be obtained at the discretion of the Geotechnical Engineering firm but to a minimum of one test for every 500 cubic yards placed and/or for every 2 feet of compacted fill placed.

The minimum relative compaction shall be obtained in accordance with accepted methods in the construction industry. The final grade of the structural areas shall be in a dense and smooth condition prior to placement of slabs-on-grade or pavement areas. No fill soils shall be placed, spread or compacted during unfavorable weather conditions. When the grading is interrupted by heavy rains, compaction operations shall not be resumed until approved by the Geotechnical Engineering firm.

Grading Observations

The controlling governmental agencies should be notified prior to commencement of any grading operations. This firm recommends that the grading operations be conducted under the observation of a Geotechnical Engineering firm as deemed necessary. A 24-hour notice must be provided to this firm prior to the time of our initial inspection.

Observation shall include the clearing and grubbing operations to assure that all unsuitable materials have been properly removed; approve the exposed subgrade in areas to receive fill and in areas where excavation has resulted in the desired finished grade and designate areas of overexcavation; and perform field compaction tests to determine relative compaction achieved during fill placement. In addition, all foundation excavations shall be observed by the Geotechnical Engineering firm to confirm that appropriate bearing materials are present at the design grades and recommend any modifications to construct footings.

EXPANSIVE SOIL GUIDELINES

The following expansive soil guidelines are provided for your project. The intent of these guidelines is to inform you, the client, of the importance of proper design and maintenance of projects supported on expansive soils. You, as the owner or other interested party, should be warned that you have a duty to provide the information contained in the soil report including these guidelines to your design engineers, architects, landscapers and other design parties in order to enable them to provide a design that takes into consideration expansive soils.

In addition, you should provide the soil report with these guidelines to any property manager, lessee, property purchaser or other interested party that will have or assume the responsibility of maintaining the development in the future.

Expansive soils are fine-grained silts and clays which are subject to swelling and contracting. The amount of this swelling and contracting is subject to the amount of fine-grained clay materials present in the soils and the amount of moisture either introduced or extracted from the soils. Expansive soils are divided into five categories ranging from "very low" to "very high". Expansion indices are assigned to each classification and are included in the laboratory testing section of this report. If the expansion index of the soils on your site, as stated in this report, is 21 or higher, you have expansive soils. The classifications of expansive soils are as follows:

Classification of Expansive Soil*

Expansion Index		Potential Expansion
	0-20	Very Low
	21-50	Low
	51-90	Medium
	91-130	High
	Above 130	Very High

*From Table 18A-I-B of California Building Code (1988)

When expansive soils are compacted during site grading operations, care is taken to place the materials at or slightly above optimum moisture levels and perform proper compaction operations. Any subsequent excessive wetting and/or drying of expansive soils will cause the soil materials to expand and/or contract. These actions are likely to cause distress of foundations, structures, slabs-on-grade, sidewalks and pavement over the life of the structure. It is therefore imperative that even after construction of improvements, the moisture contents are maintained at relatively constant levels, allowing neither excessive wetting or drying of soils.

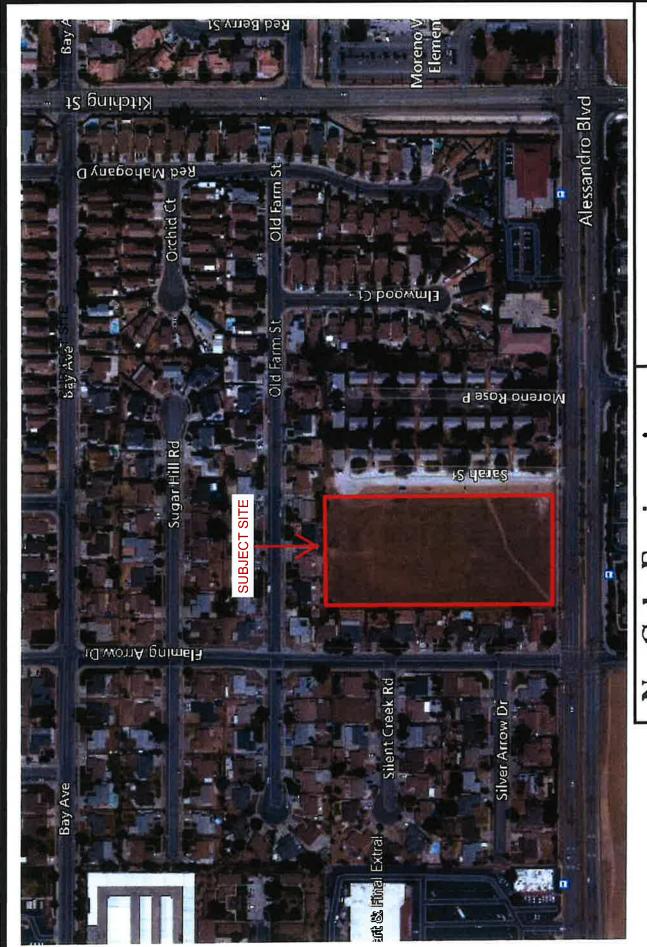
Evidence of excessive wetting of expansive soils may be seen in concrete slabs, both interior and exterior. Slabs may lift at construction joints producing a trip hazard or may crack from the pressure of soil expansion. Wet clays in foundation areas may result in lifting of the structure causing difficulty in the opening and closing of doors and windows, as well as cracking in exterior and interior wall surfaces. In extreme wetting of soils to depth, settlement of the structure may eventually result. Excessive wetting of soils in landscape areas adjacent to concrete or asphaltic pavement areas may also result in expansion of soils beneath pavement and resultant distress to the pavement surface.

Excessive drying of expansive soils is initially evidenced by cracking in the surface of the soils due to contraction. Settlement of structures and on-grade slabs may also eventually result along with problems in the operation of doors and windows.

Projects located in areas of expansive clay soils will be subject to more movement and "hairline" cracking of walls and slabs than similar projects situated on non-expansive sandy soils. There are, however, measures that developers and property owners may take to reduce the amount of movement over the life the development. The following guidelines are provided to assist you in both design and maintenance of projects on expansive soils:

- Drainage away from structures and pavement is essential to prevent excessive wetting of expansive soils. Grades should be designed to the latest building code and maintained to allow flow of irrigation and rain water to approved drainage devices or to the street. Any "ponding" of water adjacent to buildings, slabs and pavement after rains is evidence of poor drainage; the installation of drainage devices or regrading of the area may be required to assure proper drainage. Installation of rain gutters is also recommended to control the introduction of moisture next to buildings. Gutters should discharge into a drainage device or onto pavement which drains to roadways.
- Irrigation should be strictly controlled around building foundations, slabs and
 pavement and may need to be adjusted depending upon season. This control is
 essential to maintain a relatively uniform moisture content in the expansive soils and
 to prevent swelling and contracting. Over-watering adjacent to improvements may
 result in damage to those improvements. NorCal Engineering makes no specific
 recommendations regarding landscape irrigation schedules.
- Planting schemes for landscaping around structures and pavement should be analyzed carefully. Plants (including sod) requiring high amounts of water may result in excessive wetting of soils. Trees and large shrubs may actually extract moisture from the expansive soils, thus causing contraction of the fine-grained soils.
- Thickened edges on exterior slabs will assist in keeping excessive moisture from entering directly beneath the concrete. A six-inch thick or greater deepened edge on slabs may be considered. Underlying interior and exterior slabs with 6 to 12 inches or more of non-expansive soils and providing presaturation of the underlying clayey soils as recommended in the soil report will improve the overall performance of ongrade slabs.

- Increase the amount of steel reinforcing in concrete slabs, foundations and other structures to resist the forces of expansive soils. The precise amount of reinforcing should be determined by the appropriate design engineers and/or architects.
- Recommendations of the soil report should always be followed in the development of the project. Any recommendations regarding presaturation of the upper subgrade soils in slab areas should be performed in the field and verified by the Soil Engineer.



VICINITY MAP

NorCal Engineering SOILS AND GEOTECHNICAL CONSULTANTS

TRAN CHUNG

DATE: AUGUST 2021

PROJECT: 22686-21





NorCal Engineering soils and Geotechnical Consultants

TRAN CHUNG

PROJECT 22686-21

DATE AUGUST 2021

SITE PLAN

List of Appendices

(in order of appearance)

Appendix A – Log of Excavations

Log of Borings T-1 to T-10

Appendix B – Laboratory Tests

Table I – Maximum Dry Density Table II – Expansion Table III – Atterberg Limits Table IV - Corrosion Plate A - Direct Shear Plates B and C - Consolidation

Appendix C Seismic Design

ASCE Seismic Hazards Report Moreno Valley Geological Faults and Liquefaction Map

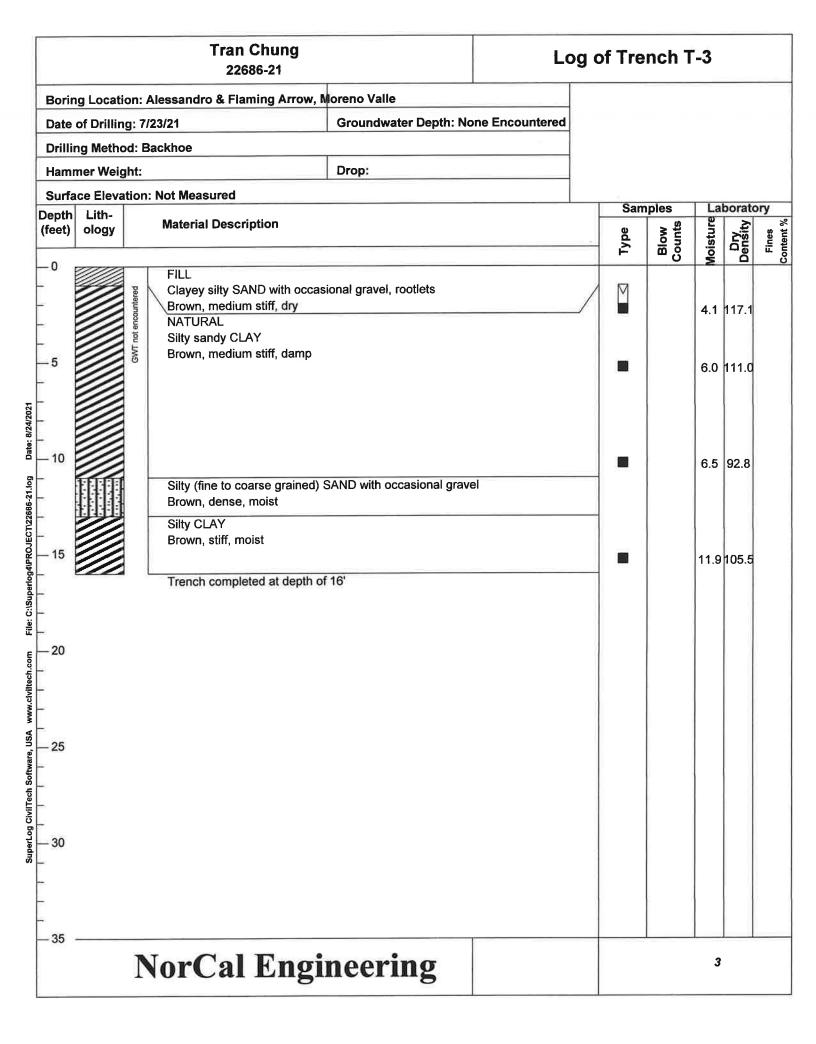
Appendix D – Soil Infiltration

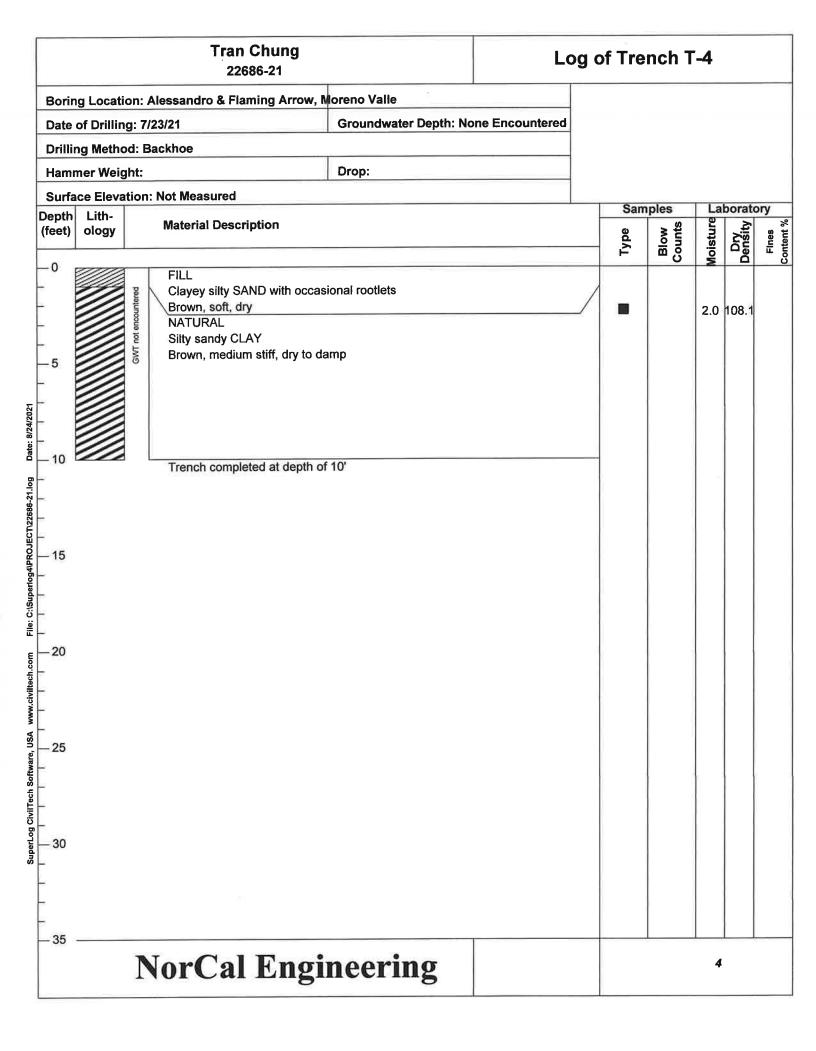
Soil Infiltration Data

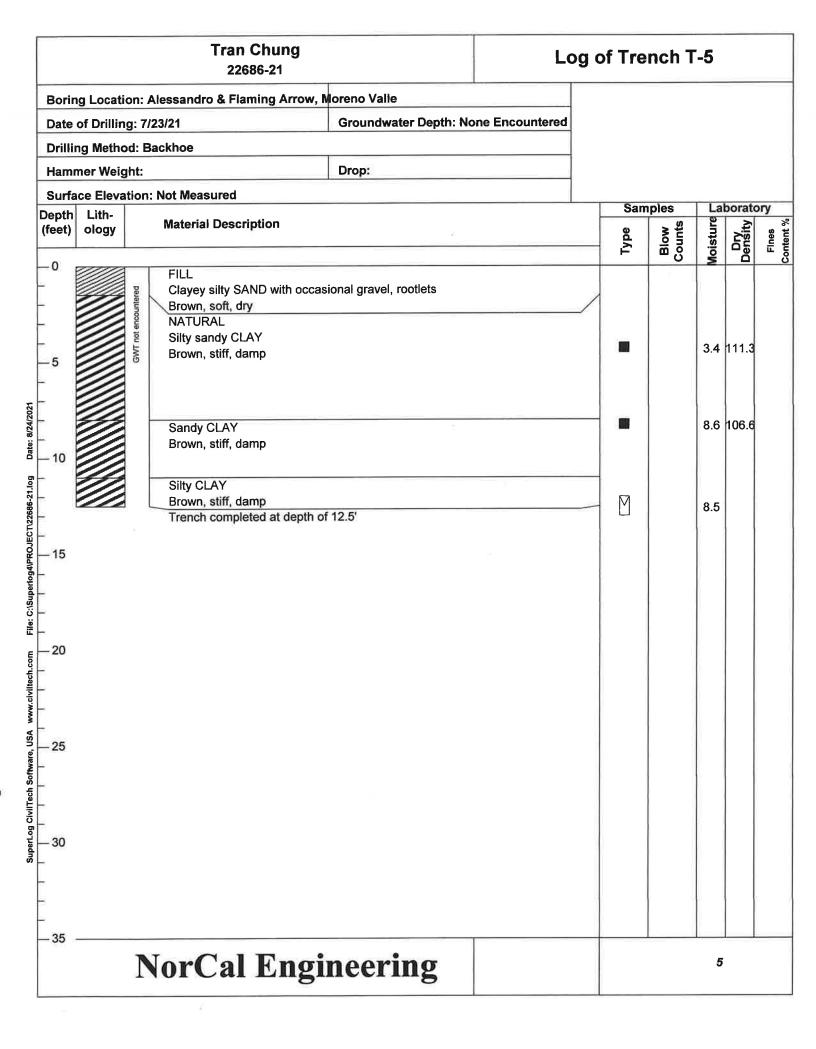
Appendix A Log of Excavations

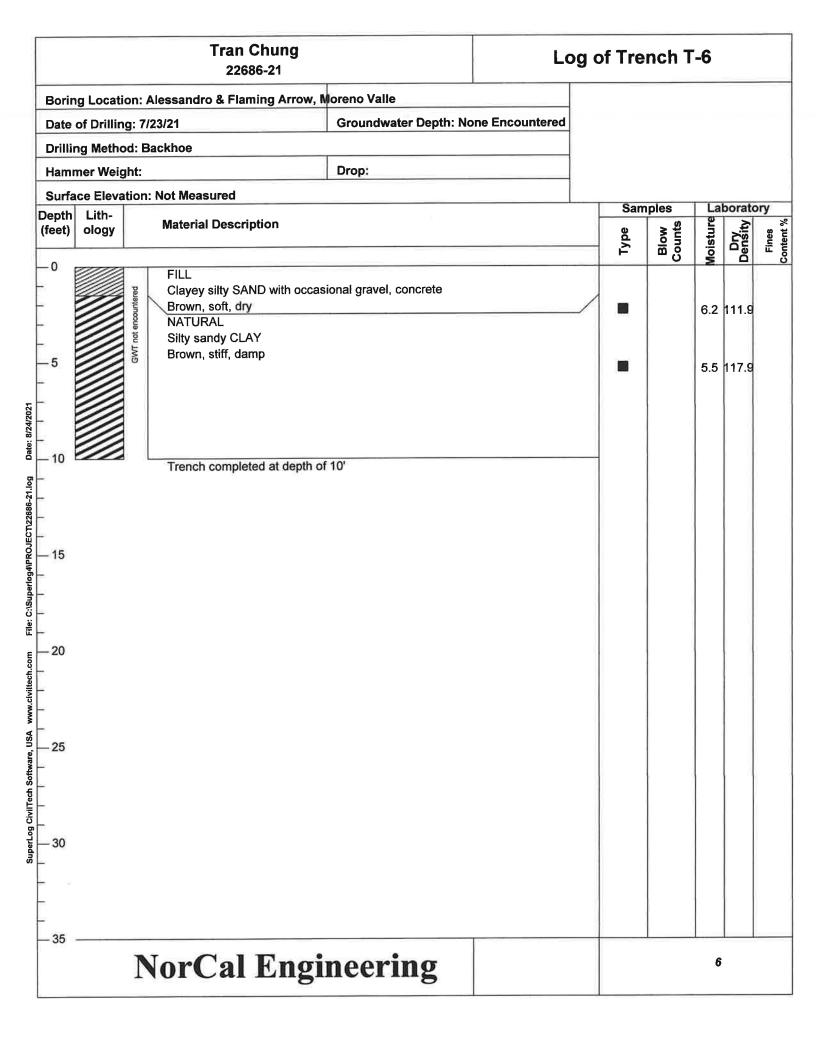
	Tran Chung 22686-21		Log	of Tre	nch T	·-1		
Boring Loc	cation: Alessandro & Flaming Arrow, N	loreno Valle						
Date of Dr	illing: 7/23/21	Groundwater Depth: No	one Encountered					
Drilling Me	thod: Backhoe							
Hammer V	/eight:	Drop:						
	evation: Not Measured			Sam	ples	2	oorate	on/
Depth Lith						5		» ×
	"			Туре	Blow	Moisture	Dry Density	Fines Content %
- 0	FILL Clayey silty SAND with occass Brown, medium stiff, dry NATURAL Silty sandy CLAY Brown, stiff, damp Trench completed at depth of							
_35	NorCal Engi	neering			1	1		

		Tran Chung 22686-21	_	Lo	g of Tre	nch T	-2		
Boriı	ng Locat	on: Alessandro & Flaming Arrow, I	oreno Valle						
Date	of Drillin	g: 7/23/21	Groundwater Depth: No	one Encountered					
Drilli	ing Metho	od: Backhoe	-						
Ham	mer Wei	jht:	Drop:						
		tion: Not Measured			Sam	ples	l l a	borate	orv.
Depth (feet)		Material Description							» ±
					- Type	Blow	Moisture	Dry Density	Fines Content %
SuperLog Civil Tech Software, USA www.civiltech.com File: C:Superlog4l/ROJEC172666-21.log Date: 6/24/2021		FILL Clayey silty SAND with occass Brown, medium stiff, dry NATURAL Silty sandy CLAY Brown, stiff, damp Silty (fine to coarse grained) and service states are serviced at depth of services and services are services are services and services are services and services are services are services and services are service	SAND with occasional grave	el					
- 35	D L	NorCal Engi	neering			•	2		









		Tran Chung 22686-21		Lo	og of Tre	nch T	- -7		
Borir	ng Locat	on: Alessandro & Flaming Arrow, N	loreno Valle						
Date	of Drillir	g: 7/23/21	Groundwater Depth: No	ne Encountered					
Drilli	ng Meth	od: Backhoe							
Hami	mer Wei	jht:	Drop:						
Surfa	ace Eleva	ition: Not Measured							
Depth		Material Description				nples	La <u>e</u>	oorate	ory *
(feet)	ology				Type	Blow	Moisture	Dry Density	Fines Content %
-0 - - - -5 - - -10 - - -15 - - - -20 - - - - - - - - - - - - - - -		FILL Clayey silty SAND with occass Brown, soft, dry NATURAL Silty sandy CLAY Brown, stiff, damp Silty (fine to coarse grained) S Brown, dense, damp Trench completed at depth of	SAND with occasional grave					114.3	8
— 35		NorCal Engi	neering				7		

	Tran Chung 22686-21		Log	of Tre	nch T	-8		
Boring Location: Alessan	dro & Flaming Arrow, M	oreno Valle						
Date of Drilling: 7/23/21		Groundwater Depth: No	ne Encountered					
Drilling Method: Backhoe								
Hammer Weight:		Drop:						
Surface Elevation: Not Me	easured			Sam	ples	Lat	orato	orv
Depth Lith- (feet) ology Mater	rial Description			Туре	Blow	Moisture	Dry Density	Fines Content %
Brown NAT Silty Brown Tren	ey silty SAND with occasion, medium stiff, dry URAL sandy CLAY vn, stiff, damp ch completed at depth of	5'			GO		114.3	Fi
Nor	Cal Engi	neering				8		

	Tran Chung 22686-21	Log	of Tren	ch T	-9		
Boring Location: Alessandre	& Flaming Arrow, Moreno Valle						
Date of Drilling: 7/23/21	Groundwater Dept	th: None Encountered					
Drilling Method: Backhoe							
Hammer Weight:	Drop:						
Surface Elevation: Not Meas	ured		Samp	les	Lak	orato	rv
Depth Lith- (feet) ology Material	Description			Blow	Moisture	Density	Fines Content %
Brown, NATUR Silty sa Brown, Silty sa Brown,	ndy CLAY medium stiff, damp ne to coarse grained) SAND with occasional	gravel		9		111.8	0
SuperLog Civil Tech Software, USA www.civilitech.com File: C:SuperlogAlPROJECT/22886-21.log	dense, damp completed at depth of 10'						
NorC	Cal Engineering				9		

Tran Chung 22686-21		Log of	Trer	ich T-	10		
Boring Location: Alessandro & Flaming Arr	ow, Moreno Valle						
Date of Drilling: 7/23/21	Groundwater Depth: No	one Encountered					
Drilling Method: Backhoe							
Hammer Weight:	Drop:						
Surface Elevation: Not Measured			Sam	nlae	ادا	orate	on/
Depth Lith-			= ===				ر پر چ
(1823) 51233			Туре	Blow	Moisture	Dry Density	Fines Content %
FILL Clayey silty SAND with Brown, medium stiff, dry NATURAL Silty sandy CLAY Brown, stiff, dry to damp Trench completed at de)				1.3	116.7 114.6	
NorCal En	gineering				10)	

Appendix B Laboratory Tests

TABLE I MAXIMUM DENSITY TESTS

Sample	Classification	Optimum Moisture (%)	Maximum Dry Density (lbs/cu.ft)
T3 @ 1'	Silty Sandy CLAY	10.5	128.0

TABLE II EXPANSION TESTS

Sample	Classification	Expansion Index
T3 @ 1'	Silty Sandy CLAY	33

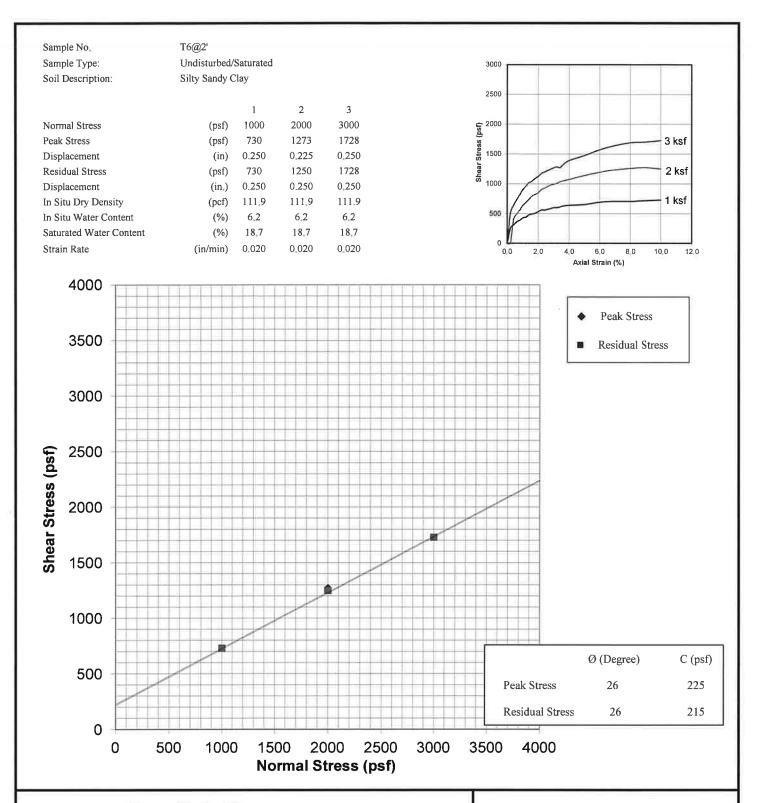
TABLE III ATTERBERG LIMITS

Sample	Liquid Limit	Plastic Limit	Plasticity Index
T-3 @ 5'	18	17	1
T-3 @ 10'	26	17	9

TABLE IV CORROSION TESTS

Sample	рН	Electrical Resistivity	Sulfate (%)	Chloride (ppm)
T-3 @ 1'	7.0	15,320	N.D.	111

% by weight ppm – mg/kg N.D. = Non-Detect



NorCal Engineering

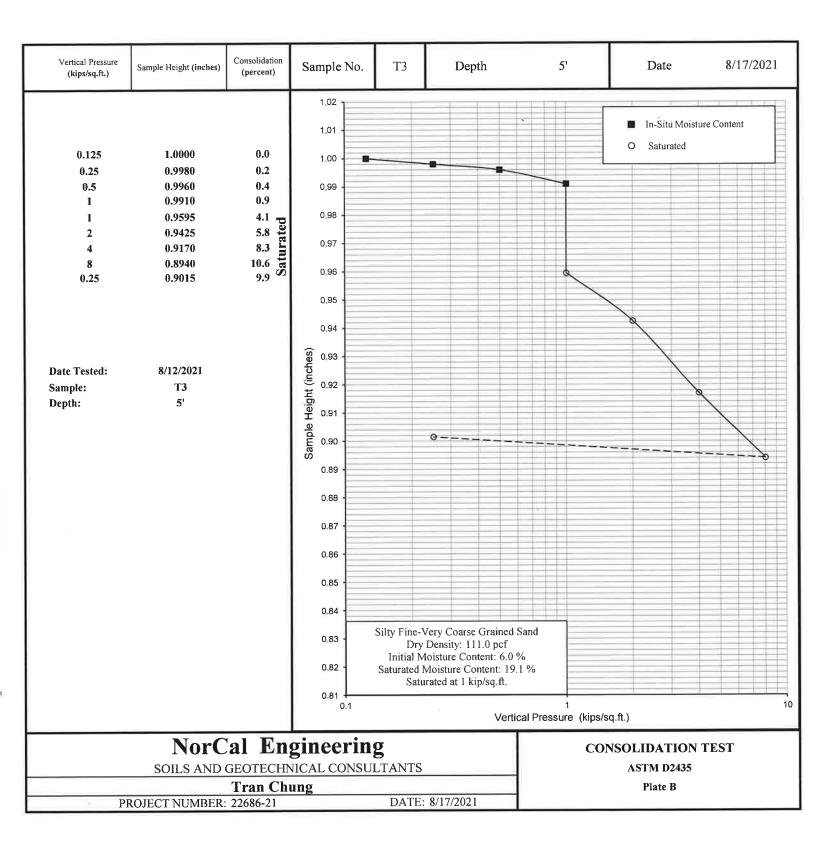
SOILS AND GEOTECHNICAL CONSULTANTS

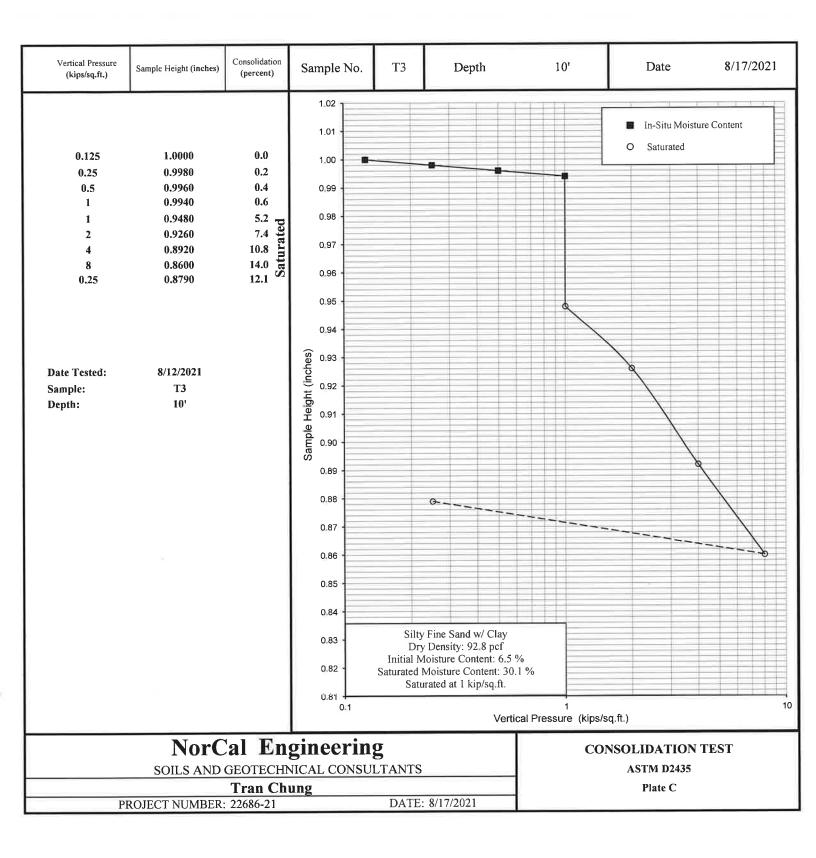
Tran Chung

PROJECT NUMBER: 22686-21

DATE: 8/17/2021

DIRECT SHEAR TEST
ASTM D3080
Plate A







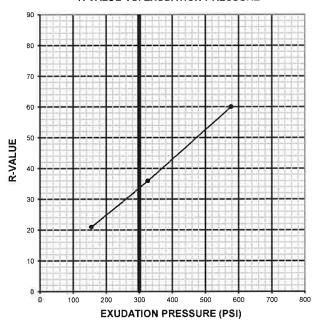
R-VALUE TEST REPORT

☑ CT-301 ☐ ASTM-D2844

PROJECT NAME;	Norcal: Tran Cheng 22686-21	PROJECT NUMBER:	L-210801
SAMPLE LOCATION:	N of Alessandro Boulevard and E of Flaming Arrow Drive, Moreno Valley	SAMPLE NUMBER:	T1
SAMPLE DESCRIPTION:	CLAYEY SAND (SC), brown	SAMPLE DEPTH:	2'
SAMPLED BY:	Norcal 7/23/21	TESTED BY:	ER
		DATE TESTED:	8/8/2021

TEST SPECIMEN	A	В	С
MOISTURE AT COMPACTION %	8.7	9.7	10.7
WEIGHT OF SAMPLE, grams	1042	1086	1124
HEIGHT OF SAMPLE, Inches	2.33	2.35	2.48
DRY DENSITY, pcf	124.8	127.7	124.1
COMPACTOR AIR PRESSURE, psi	280	220	130
EXUDATION PRESSURE, psi	577	326	155
EXPANSION, Inches x 10exp-4	38	13	3
STABILITY Ph 2,000 lbs (160 psi)	40	72	100
TURNS DISPLACEMENT	4.07	4.68	5.80
R-VALUE UNCORRECTED	65	40	21
R-VALUE CORRECTED	60	36	21
EXPANSION PRESSURE (psf)	164.2	56.2	13.0

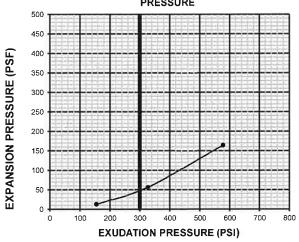
R-VALUE VS. EXUDATION PRESSURE

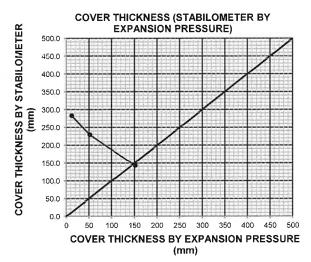


R-VALUE AT EQUILIBRIUM:	33
-------------------------	----

R-VALUE BY EXUDATION PRESSURE:	33
R-VALUE BY EXPANSION PRESSURE:	58
EXPANSION PRESSURE AT 300 PSI EXUDATION:	45
TRAFFIC INDEX (Assumed):	5.5
GRAVEL FACTOR (Assumed):	1.5
UNIT MASS OF COVER MATERIAL, kg/m^3 (Assumed):	2100.0

EXPANSION PRESSURE VS. EXUDATION PRESSURE





Appendix C Seismic Hazard Report



Address:

No Address at This Location

ASCE 7 Hazards Report

Standard: ASCE/SEI 7-16

Risk Category: ||

Soil Class: D - Stiff Soil

Elevation: 1566.66 ft (NAVD 88)

Latitude: 33.918062 **Longitude:** -117.221483







Seismic

Site Soil Class: D - Stiff Soil

Results:

S_s: 1.653 S_{D1} : N/A T_L : S₁: 0.644 8 Fa: 1 PGA: 0.7 PGA M: F_v: N/A 0.77 F_{PGA} : S_{MS} : 1.653 1.1 S_{M1} : N/A 1.102 C_v : 1.431 S_{DS} :

Ground motion hazard analysis may be required. See ASCE/SEI 7-16 Section 11.4.8.

Data Accessed:

Wed Aug 25 2021

Date Source:

USGS Seismic Design Maps



The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.

Geologic Faults and Liquefaction Emergency Operations Center Potential Liquefaction

March Air Reserve Ber
City of Moreno Valley

Surrounding Cities Public Safety Building MORENO Fire Station Fault Zone CALINESA Pre Staton 91 (Cotege Part) March Air Reserve Base RNERSIDE

Figure 4-1.1: Moreno Valley Geologic Faults and Liquefaction



Appendix D Soil Infiltration Data



SOILS AND GEOTECHNICAL CONSULTANTS

Project: Tran Chung
Project No.: 22686-21
Date: 7/23/2021
Test No. 1
Depth: 5'
Tested By: D.L.

TIME (hr/min)	CHANGE TIME (min)	CUMULATIVE TIME (min)	INNER RING READING (cm)	INNER RING CHANGE	INNER RING FLOW (cc)	OUTER RING READING (cm)	OUTER RING CHANGE	OUTER RING FLOW (cc)	INNER RING INF RATE (cm/hr)	OUTER RING INF RATE (cm/hr)	INNER RING INF RATE (ft/hr)
7:58			100.7			37.6					
8:13	15	15	101.6	0.9		38.1	0.5				
8:13			101.6			38.1					
8:28	15	30	102.6	1.0		38.6	0.5				
8:28			102.6			38.6					
8:43	15	45	103.6	1.0		39.3	0.7				
8:43			103.6			39.3					
8:58	15	60	104.4	0.8		40.0	0.7				
8:58			104.4			40.0					
9:13	15	75	105.1	0.7		40.6	0.6				
9:13			105.1			40.6					
9:28	15	90	105.9	0.8		41.1	0.5				
9:28			105.9			41.1					
9:43	15	105	106.6	0.7		41.7	0.6		2.8	2.4	
9:43			104.2			40.6					
9:58	15	120	104.6	0.4		41.1	0.5		1.6	2.0	
9:58			104.6			41.1					
10:13	15	135	104.9	0.3		41.5	0.4		1.2	1.6	
10:13			104.9			41.5					
10:28	15	150	105.2	0.3		41.9	0.4		1.2	1.6	
10:28			105.2			41.9					
10:43	15	165	105.4	0.2		42.3	0.4		0.8	1.6	
10:43			105.4			42.3					
10:58	15	180	105.2	0.3		42.9	0.6		1.2	2.4	

Average = 1.46 / 1.93 cm/hr



SOILS AND GEOTECHNICAL CONSULTANTS

Project: Tran Chung
Project No.: 22686-21
Date: 7/23/2021
Test No. 2
Depth: 10'
Tested By: D.L.

TIME (hr/min)	CHANGE TIME (min)	CUMULATIVE TIME (min)	INNER RING READING (cm)	INNER RING CHANGE	INNER RING FLOW (cc)	OUTER RING READING (cm)	OUTER RING CHANGE	OUTER RING FLOW (cc)	INNER RING INF RATE (cm/hr)	OUTER RING INF RATE (cm/hr)	INNER RING INF RATE (ft/hr)
9:09			132.1			42.0					
9:24	15	15	132.5	0.4		43.0	1.0				
9:24			132.5			43.0					
9:39	15	30	133.0	0.5		43.8	0.8				
9:39			133.0			43.8					
9:54	15	45	133.6	0.6		44.7	0.9				
9:54			133.6			44.7					
10:09	15	60	134.2	0.6		45.5	0.8				
10:09			134.2			45.5					
10:24	15	75	134.4	0.2		46.1	0.6				
10:24			134.4			46.1					
10:39	15	90	137.7	0.3		46.8	0.7				
10:39			137.7			46.8					
10:54	15	105	138.1	0.4		47.5	0.7		1.6	2.8	
10:54			138.1			47.5					
11:09	15	120	138.5	0.4		48.1	0.6		1.6	2.4	
11:09			138.5			48.1					
11:24	15	135	138.8	0.3		48.8	0.7		1.2	2.8	
11:24			128.8			41.2		1			
11:39	15	150	129.1	0.3		42.1	0.9		1.2	3.6	
11:39			129.1			42.1					
11:54	15	165	129.6	0.6		42.9	0.8		2.4	3.2	
11:54			129.6			42.9					
12:09	15	180	130.0	0.4		43.5	0.6		1.6	2.4	

Average = 1.6 / 2.86 cm/hr

Appendix 4: Historical Site Conditions

Phase I Environmental Site Assessment or Other Information on Past Site Use

Appendix 5: LID Infeasibility

LID Technical Infeasibility Analysis

Appendix 6: BMP Design Details

BMP Sizing, Design Details and other Supporting Documentation

	Santa	Ana Wat	ershed - BMP I	Design Vo	lume, V _B	SMP	Legend:		Required Entri
			(Rev. 10-2011)						Calculated Cel
			heet shall <u>only</u> be used	in conjunction	n with BMP	designs from the	LID BMP I		
_	y Name	Waber Consu							10/20/2022
Designe			P.E., LEED AP		21026374	LLEVCARE	ENIC	Case No	LWQ21-0055
ompan	y Project	Number/Name	2		21036 VA	LLEY GARD	DENS		
				BMP I	dentificati	on			
MP N	AME / ID	AREA - 1	Mus	t match Nan	ne/ID used /	on BMP Design	Calculation	Sheet	
			IVIUS		Rainfall De		Carcaration	Silect	
		l-hour Rainfal Map in Hand	l Depth, book Appendix E	Design		.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	D ₈₅ =	0.67	inches
Drainage Management Area Tabulation									
_		Ir	sert additional rows	if needed to	accommodo	ate all DMAs dro	aining to th	е ВМР	
	DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Imperivous Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
							- op ()	(carry cos)	yeay
	Area - 1	7132	Mixed Surface Types	0.46	0.31	2243.1			
		7132	7	otal		2243.1	0.67	125.2	140
lotes:									

	Santa	Ana Wat	ershed - BMP 1	Design Vo	lume, $V_{\rm B}$	BMP	Legend:		Required Ent	
		(Note this works	heet shall <u>only</u> be used	in conjunction	n with BMP	designs from the	LID BMP I	Design Handbook)	
Compan	-	Waber Consu						Date	10/20/2022	
Designe			r P.E., LEED AP					Case No	LWQ21-005	5
Compan	y Project	Number/Name	e		21036 VA	LLEY GARD	DENS			
				BMP I	dentificati	on				
BMP N	AME / ID	AREA - 2								
			Mus	t match Nan	ne/ID used o	on BMP Design	Calculation	Sheet		
				Design l	Rainfall De	epth				
		l-hour Rainfal Map in Hand	l Depth, book Appendix E				D ₈₅ =	0.67	inches	
			Drair	nage Manag	ement Are	a Tabulation				
		Ir	nsert additional rows	if needed to	accommodo	ate all DMAs dr	aining to th	е ВМР		
	DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Imperivous Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)	
	Area - 2	16281	Mixed Surface Types	0.427	0.30	4804.2				
		16281	7	otal		4804.2	0.67	268.2	294	1
NT 4										
Notes:										

	Santa	Ana Wat	ershed - BMP I	Design Vo	lume, V _B	SMP	Legend:		Required Entri
			(Rev. 10-2011)						Calculated Cell
			heet shall <u>only</u> be used	in conjunction	n with BMP	designs from the	LID BMP I		
_	y Name	Waber Consu							10/20/2022
Designe			P.E., LEED AP		21026374	LLEVCARE	ENIC	Case No	LWQ21-0055
ompan	y Project	Number/Name	2		21036 VA	LLEY GARD	JENS		
				BMP I	dentificati	on			
MP NA	AME / ID	AREA - 3	NA.	et match Nan	aa/ID usad	on BMP Design	Calculation	Shoot	
			ivius		Rainfall De		Carculation	SHEEL	
		l-hour Rainfal Map in Hand	l Depth, book Appendix E	Design	Kumum DV		D ₈₅ =	0.67	inches
			Drair	nage Manag	ement Are	a Tabulation			
_		Ir	sert additional rows	if needed to	accommodo	ate all DMAs dr	aining to th	е ВМР	
	DMA Type/ID	DMA Area (square feet)	Post-Project Surface	Effective Imperivous	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
			Туре	Fraction, I _f			рерин (ш)	(cubic feet)	Jeet)
	Area - 3	8349	Mixed Surface Types	0.451	0.31	2580.9			
ŀ									
-									
-									
ŀ									
ŀ									
ŀ									
		8349	7	otal		2580.9	0.67	144.1	171.5
				-		1 3 5 10			-
otes:									

			ershed - BMP I				Legend:		Required Entries Calculated Cells	
			heet shall <u>only</u> be used	in conjunction	n with BMP o	designs from the	LID BMP I			
Compan		Waber Consu							10/20/2022	
Designe		Number/Name	P.E., LEED AP		21036 VA	LLEY GARD	ENC	Case No	LWQ21-0055	
Compan	ly Project	INUIIIDEI/INAIII	-		21030 VA	LLET GARL	LINS			
				BMP I	dentification	on				
BMP N	BMP NAME / ID AREA - 4									
	Must match Name/ID used on BMP Design Calculation Sheet									
	Design Rainfall Depth									
85th Percentile, 24-hour Rainfall Depth, $D_{85} = 0.67$ inches from the Isohyetal Map in Handbook Appendix E										
	Drainage Management Area Tabulation									
		Ir	sert additional rows				aining to th	е ВМР		
	DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Imperivous Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)	
	Area - 4	20137	Mixed Surface Types	0.878	0.70	14075.9				
		20137	7	otal		14075.9	0.67	785.9	799	
Notes:										

	Santa	Ana Wat	ershed - BMP I	Design Vo	lume, V_B	MP	Legend:		Required Entr		
		(Note this works	heet shall <u>only</u> be used	in conjunction	n with BMP o	designs from the	LID BMP D				
Compan	-	Waber Consu	<u> </u>						10/20/2022		
Designe			P.E., LEED AP					Case No	LWQ21-0055		
Compan	y Project	Number/Name	e		21036 VA	LLEY GARD	DENS				
				BMP I	dentification	on					
BMP N	AME / ID	AREA - 5									
	Must match Name/ID used on BMP Design Calculation Sheet										
	Design Rainfall Depth										
85th Percentile, 24-hour Rainfall Depth, $D_{85} = 0.67$ inches from the Isohyetal Map in Handbook Appendix E											
	Drainage Management Area Tabulation										
ı		Ir	sert additional rows	if needed to (accommoda	te all DMAs dr	aining to the	e BMP			
	DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Imperivous Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)		
	Area - 5	52491	Mixed Surface Types	0.836	0.64	33764					
		52491	7	otal		33764	0.67	1885.2	2025		
Notes:											

			ershed - BMP I				Legend:		Required Entries Calculated Cells	
_			heet shall <u>only</u> be used	in conjunction	n with BMP o	designs from the	LID BMP I			
Compan		Waber Consu							10/20/2022	
Designe		Number/Name	P.E., LEED AP		21036 VA	LLEY GARD	ENC	Case No	LWQ21-0055	
Compan	ly Project	INUIIIDEI/INAIII	5		21030 VA	LLET GARL	LINS			
				BMP I	dentification	on				
BMP N	BMP NAME / ID AREA - 6									
	Must match Name/ID used on BMP Design Calculation Sheet									
	Design Rainfall Depth									
85th Percentile, 24-hour Rainfall Depth, from the Isohyetal Map in Handbook Appendix E D_{85} inches										
			Drair	age Manag	ement Are	a Tabulation				
		Ir	sert additional rows				ainina to th	e BMP		
	DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Imperivous Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)	
	Area - 6	6208	Mixed Surface Types	0.577	0.39	2431.9				
			,,,,,,							
		6208	7	otal		2431.9	0.67	135.8	141.75	
Notes:										

	Santa	Ana Wat	<mark>ershed</mark> - BMP I	Design Vo	lume, V _B	SMP	Legend:		Required Entr
			(Rev. 10-2011)						Calculated Ce
7			heet shall <u>only</u> be used	in conjunction	n with BMP	designs from the	LID BMP L		10/20/2022
ompan Designe	y Name	Waber Consu	P.E., LEED AP						LWQ21-0055
		Number/Name			21036 VA	LLEY GARD	ENS	Case No	LWQ21-0033
ompun	y 110ject	r (dilio di) i (dili	9		21030 111	ELLI GIITE	EITE		
				BMP I	dentificati	on			
MP N	AME / ID	AREA - 7							
			Mus	t match Nan	ne/ID used (on BMP Design	Calculation	Sheet	
				Design l	Rainfall De	epth			
		1-hour Rainfal Map in Hand	l Depth, book Appendix E				D ₈₅ =	0.67	inches
			Drair	nage Manag	ement Are	a Tabulation			
ı		Ir	sert additional rows	if needed to	accommodo	nte all DMAs dro	aining to the	e BMP	
	DMA	DMA Area	Post-Project Surface	Effective Imperivous	DMA Runoff	DMA Areas x	Design Storm	Design Capture Volume, V _{BMP}	Proposed Volume on Plans (cubic
	Type/ID	(square feet)	Туре	Fraction, I _f	Factor	Runoff Factor	Depth (in)	(cubic feet)	feet)
	Area - 7	4622	Mixed Surface Types	0.734	0.53	2436.6			
		4622	7	otal		2436.6	0.67	136	141
-4-									
otes:									

	<u>Santa</u>	Ana Wat	ershed - BMP I	SMP	Legend:		Required Ent					
		(Note this works	heet shall <u>only</u> be used	in conjunction	n with BMP	designs from the	LID BMP L	Design Handbook				
Compar	ny Name	Waber Const	ıltants, Inc.	•				Date	10/20/2022			
Designe			r P.E., LEED AP					Case No	LWQ21-0055	5		
Compar	ny Project I	Number/Nam	e		21036 VA	LLEY GARE	DENS					
				BMP I	dentificati	on						
BMP N	AME / ID	AREA - 8										
			Mus	st match Nan	ne/ID used (on BMP Design	Calculation	Sheet				
				Design l	Rainfall De	epth						
	85th Percentile, 24-hour Rainfall Depth, $D_{85} = 0.67$ inches from the Isohyetal Map in Handbook Appendix E											
	Drainage Management Area Tabulation											
		Ir	nsert additional rows	if needed to	accommodo	ate all DMAs dr	aining to the	е ВМР		ĺ		
	DMA DMA Area Type/ID (square feet) Post-Project Surface Effective Type Fraction, I _f Factor Factor Runoff Factor Design Design Capture Volume on Plans (cubic feet) Proposed Pro											
	Area - 8	13004	Mixed Surface Types	0.517	0.35	4554.5						
			, ,,									
		12004	7	'atal		4554.5	0.67	254.2	262			
		13004	ı '	otal		4554.5	0.67	254.3	262	l		
Notes:												

Santa Ana Watershed - BMP Design Volume, V _{BMP} (Rev. 10-2011)							Legend:		Required Ent	
(Note this worksheet shall only be used in conjunction with BMP designs from the LID BMP Design Handbook)										
Compan	-	Waber Consu	<u> </u>						10/20/2022	
Designe			P.E., LEED AP					Case No	LWQ21-0055	5
Compan	y Project	Number/Name	e		21036 VA	LLEY GARD	DENS			
BMP Identification										
BMP NAME / ID AREA - 9										
			Mus	t match Nan	ne/ID used o	on BMP Design	Calculation	Sheet		
Design Rainfall Depth										
85th Percentile, 24-hour Rainfall Depth, from the Isohyetal Map in Handbook Appendix E							D ₈₅ =	0.67	inches	
Drainage Management Area Tabulation										
ı	Insert additional rows if needed to accommodate all DMAs draining to the BMP									
	DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Imperivous Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)	
	Area - 9	16061	Mixed Surface Types	0.446	0.31	4917.4				
			7,11			10 = 111				
		16061	7	otal		4917.4	0.67	274.6	278	
Notes:										
INUIES:										

	Santa	Ana Wat	ershed - BMP 1	Design Vo	lume, $V_{\rm B}$	BMP	Legend:		Required Entr	
			heet shall <u>only</u> be used	in conjunction	n with BMP	designs from the	LID BMP I			
Compan		Waber Const							10/20/2022	
Designe			r P.E., LEED AP		01006771			Case No	LWQ21-0055	
Compan	y Project	Number/Nam	e		21036 VA	LLEY GARD	DENS			
				BMP I	dentificati	on				
BMP N	AME / ID	AREA - 10								
			Mus	t match Nan	ne/ID used o	on BMP Design	Calculation	Sheet		
				Design l	Rainfall De	epth				
		l-hour Rainfal Map in Hand	l Depth, book Appendix E				D ₈₅ =	0.67	inches	
			Drair	nage Manag	ement Are	a Tabulation				
		Ir	nsert additional rows	if needed to	accommodo	ate all DMAs dr	aining to th	е ВМР		
	DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Imperivous Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)	
	Area - 10	6166	Mixed Surface Types	0.533	0.36	2225.1				
		6166	7	otal		2225.1	0.67	124.2	141 75	
		6166	l '	otai		2225.1	0.67	124.2	141.75	
Notes:										

	·		ershed - BMP I				Legend:		Required Entries Calculated Cells
			heet shall <u>only</u> be used	in conjunction	n with BMP o	designs from the	LID BMP L		
Compan		Waber Consu							10/20/2022
Designe		Number/Name	P.E., LEED AP		21036 VA	LLEY GARD	ENC	Case No	LWQ21-0055
Compan	ly Project	Nullioei/Ivallio	5		21030 VA	LLET GARL	LINO		
				BMP I	dentification	on			
BMP N	AME / ID	AREA - 11							
			Mus	t match Nan	ne/ID used o	on BMP Design	Calculation	Sheet	
				Design l	Rainfall De	epth			
		l-hour Rainfal Map in Hand	l Depth, book Appendix E				D ₈₅ =	0.67	inches
			Drair	nage Manag	ement Are	a Tabulation			
		Ir	sert additional rows				aining to the	е ВМР	
	DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Imperivous Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
	Area - 11	4491	Mixed Surface Types	0.662	0.46	2063.5			
			, , ,						
		4491	7	otal		2063.5	0.67	115.2	115.3
Notes:									

	Santa	Ana Wat	ershed - BMP I	Design Vo	lume, V _B	SMP	Legend:		Required Entri
			(Rev. 10-2011)						Calculated Cell
C			heet shall <u>only</u> be used	in conjunction	n with BMP	designs from the	LID BMP L		
_	y Name	Waber Consu							10/20/2022
Designe Compan		Number/Name	P.E., LEED AP		21026 VA	LLEY GARD	ENIC	Case No	LWQ21-0055
Compan	ly I Toject	Nullioci/Inallio	_		21030 VA	LLET GARL	LINS		
				BMP I	dentificati	on			
BMP N	AME / ID	AREA - 12	Mus	t match Nan	ne/ID used (on BMP Design	Calculation	Sheet	
					Rainfall De				
		l-hour Rainfal Map in Hand	l Depth, book Appendix E	-			D ₈₅ =	0.67	inches
			Drair	nage Manag	ement Are	a Tabulation			
		Ir	sert additional rows	if needed to	accommodo	ate all DMAs dr	aining to th	е ВМР	
	DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Imperivous Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)
	Area - 12	9569	Mixed Surface Types	0.467	0.32	3050	, , ,	, , ,	, ,
			,,,,,,						
		9569	7	otal		3050	0.67	170.3	182
Notes:									
NOICS:									

	Santa	Ana Wat	ershed - BMP 1	Design Vo	lume, $V_{\scriptscriptstyle m B}$	SMP	Legend:		Required Entr	
		(Note this works	heet shall <u>only</u> be used	in conjunction	n with BMP	designs from the	LID BMP L	Design Handbook)	
Compar	ny Name	Waber Const	ıltants, Inc.	_				Date	10/20/2022	
Designe			r P.E., LEED AP					Case No	LWQ21-0055	5
Compar	ny Project 1	Number/Name	e		21036 VA	LLEY GARD	ENS			
				BMP I	dentificati	on				
BMP N	AME / ID	AREA - 13								
			Mus	st match Nan	ne/ID used (on BMP Design	Calculation	Sheet		
				Design l	Rainfall De	epth				
		l-hour Rainfal Map in Hand	l Depth, book Appendix E				D ₈₅ =	0.67	inches	
			Drair	nage Manag	ement Are	a Tabulation				
		Ir	nsert additional rows	if needed to	accommodo	ate all DMAs dr	aining to the	e BMP		i.
	DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Imperivous Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)	ĺ
	Area - 13	13708	Mixed Surface Types	0.55	0.37	5106.2				Ī
	7.1.00 10	20700	Immed surjuse Types	0.00	0.57	3100.2				Ì
										Ì
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										Ī
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										Ī
		13708	7	otal		5106.2	0.67	285.1	336	
Notes:										

	Santa	Ana Wat	ershed - BMP 1	Design Vo	lume, $V_{\rm B}$	BMP	Legend:		Required Entr	
			heet shall <u>only</u> be used	in conjunction	n with BMP	designs from the	LID BMP I			
Compan	-	Waber Const							10/20/2022	
Designe			r P.E., LEED AP		01006771			Case No	LWQ21-0055	5
Compan	y Project	Number/Nam	e		21036 VA	LLEY GARD	DENS			
				BMP I	dentificati	on				
BMP N	AME / ID	AREA - 14								
			Mus	t match Nan	ne/ID used (on BMP Design	Calculation	Sheet		
				Design l	Rainfall De	epth				
		-hour Rainfal Map in Hand	l Depth, book Appendix E				D ₈₅ =	0.67	inches	
			Drair	nage Manag	ement Are	a Tabulation				
		Ir	nsert additional rows	if needed to	accommodo	ate all DMAs dr	aining to th	е ВМР		
	DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Imperivous Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)	
	Area - 14	6330	Mixed Surface Types	0.787	0.58	3698.3				
		6220	7	otal		2600.2	0.67	206.5	206.5	
		6330	l '	otai		3698.3	0.67	200.3	206.5	
Notes:										

MP NAME	Mahir Waber Cons Mahir Waber Map in Hand	Mus Il Depth, Ibook Appendix E	BMP I st match Nan Design I	21036 VA	On On BMP Design	ENS	Design Handbook Date Case No	Calculated Cel) 10/20/2022 LWQ21-0055
esigned by ompany Produced MP NAME	Mahir Waber Cons Mahir Waber Map in Hand	Mus Ill Depth, Ibook Appendix E	BMP I st match Nan Design I	21036 VA	On On BMP Design	ENS	Date Case No	10/20/2022
esigned by ompany Produced MP NAME	Mahir Wabe ject Number/Nam / ID AREA - 15 le, 24-hour Rainfa yetal Map in Hand	Mus Il Depth, Ibook Appendix E	BMP I	<mark>dentificati</mark> ne/ID used (on on BMP Design		Case No	
MP NAME	/ ID AREA - 15 le, 24-hour Rainfa	Mus Il Depth, Ilbook Appendix E	BMP I	<mark>dentificati</mark> ne/ID used (on on BMP Design			LWQ21-0033
MP NAME	/ ID AREA - 15 le, 24-hour Rainfa yetal Map in Hand	Mus Il Depth, Ibook Appendix E	BMP I	<mark>dentificati</mark> ne/ID used (on on BMP Design		Sheet	
5th Percentil	le, 24-hour Rainfa yetal Map in Hand	ll Depth, lbook Appendix E	st match Nan Design I	ne/ID used (on BMP Design	Calculation	Sheet	
5th Percentil	le, 24-hour Rainfa yetal Map in Hand	ll Depth, lbook Appendix E	Design I			Calculation	Sheet	
	yetal Map in Hand	ll Depth, lbook Appendix E	Design I			Calculation	Sheet	
	yetal Map in Hand	lbook Appendix E	-	Rainfall De	epth			
	yetal Map in Hand	lbook Appendix E				D -	0.67	
	1	Drair				D ₈₅ =	0.67	inches
					a Tabulation			
		nsert additional rows	if needed to (accommodo	ate all DMAs dro	aining to the	e BMP	
DM		Post-Project Surface	Effective Imperivous	DMA Runoff	DMA Areas x	Design Storm	Design Capture Volume, V _{BMP}	Proposed Volume on Plans (cubic
Туре	e/ID (square feet)	Туре	Fraction, I _f	Factor	Runoff Factor	Depth (in)	(cubic feet)	feet)
Area	- 15 10244	Mixed Surface Types	0.899	0.73	7466.1			
-								
	10244	7	otal		7466.1	0.67	416.9	417
					_			
otes:								
,								

	Canta	Ana Wat	owahad DMD1	Davis VI	1 \ \ 7				Required Ent	ries
	Santa	Ana wat	(Rev. 10-2011)	Design vo	iume, V _B	SMP	Legend:		Calculated Co	
		(Note this works	heet shall <u>only</u> be used	' in conjunction	n with BMP	designs from the	LID BMP L	Design Handbook		
_	ny Name	Waber Const							10/20/2022	
Design			r P.E., LEED AP		21026374	LLEVCARD	FNG	Case No	LWQ21-0055	<u>;</u>
Compa	ny Project I	Number/Nam	ē		21036 VA	LLEY GARD	DENS			
				BMP I	dentificati	on				
BMP N	IAME / ID	AREA - 16			/ ·					
			Mus			on BMP Design	Calculation	Sheet		
				Design I	Rainfall De	epth				
		l-hour Rainfal Map in Hand	ll Depth, lbook Appendix E				D ₈₅ =	0.67	inches	
			Drair	nage Manag	ement Are	a Tabulation				
		- II	nsert additional rows	if needed to d	accommodo	ate all DMAs dro	aining to the	е ВМР		
	DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Imperivous Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)	
	Area - 16	5726	Mixed Surface Types	0.705	0.50	2855.2	Dept. (m)	(outling feet)	jecty	
			7,11							
		5726	7	otal		2855.2	0.67	159.4	169	
			•							
Notes:										
Notes:										

			ershed - BMP I				Legend:		Required Entrie	
			heet shall <u>only</u> be used	in conjunction	n with BMP	designs from the	LID BMP L			
	ny Name	Waber Consu							10/20/2022	
Designe		Number/Name	P.E., LEED AP		21036 VA	LLEY GARD	ENC	Case No	LWQ21-0055	
Compan	ly 1 loject i	Nullioci/Inallio	_		21030 VA	LLET GARL	ENS			
				BMP I	dentificati	on				
BMP N.	AME / ID	AREA - 17	Mus	st match Nan	ne/ID used (on BMP Design	Calculation	Sheet		
				Design l	Rainfall De	epth				
		l-hour Rainfal Map in Hand	l Depth, book Appendix E				D ₈₅ =	0.67	inches	
			Drair	nage Manag	ement Are	a Tabulation				
		Ir	nsert additional rows	if needed to	accommodo	nte all DMAs dro	aining to the	е ВМР		
	DMA Type/ID	DMA Area (square feet)	Post-Project Surface Type	Effective Imperivous Fraction, I _f	DMA Runoff Factor	DMA Areas x Runoff Factor	Design Storm Depth (in)	Design Capture Volume, V _{BMP} (cubic feet)	Proposed Volume on Plans (cubic feet)	
	Area - 17	10676	Concrete or Asphalt	1	0.89	9523				
		10676	7	otal		9523	0.67	531.7	532	
Notes:										

Rioretention	Facility - Desi	on Procedure	BMP ID	Legend:	Require	ed Entries	
Bioleteillion	racility - Desi	gii Procedure	Basin 1	Legena.	Calcula	ated Cells	
Company Name:		Waber Consult			Date:	20-Oct	
Designed by:		Mahir Wa		County/City (Case No.:	LWQ21-00	55
			Design Volume				
Enter the	e area tributary	to this feature			$A_T =$	0.16	acres
Enter V _I	_{BMP} determined	from Section 2	.1 of this Handbook		$V_{BMP} =$	125	ft ³
		Type of B	ioretention Facility	Design			
			r adjacent to walkways) space or Planter Boxes)				
		Bioreten	tion Facility Surface	Area			
Depth of	f Soil Filter Me	dia Layer			$d_S =$	3.0	ft
Top Wio	lth of Bioretent	ion Facility, exc	cluding curb		$\mathbf{w}_{\mathrm{T}} =$	14.0	ft
	fective Depth, $(0.3) \times d_S + (0.4)$	d _E 4) x 1 - (0.7/w _T)	+ 0.5		$d_E =$	1.75	ft
	m Surface Area $\frac{V}{V}$	***	_		$A_{M} =$	72	ft ⁻
Propose	d Surface Area	GE (10)			A=	80	ft^2
		Biorete	ention Facility Prope	rties			
Side Slo	pes in Bioreten	tion Facility			$_{\mathbf{Z}}$ =	4	:1
Diamete	r of Underdrain	1				6	inche
Longitue	linal Slope of S	Site (3% maxim	um)			0.5	%
6" Chec	x Dam Spacing					0	feet
Describe	Vegetation:	Natur	ral Grasses				
lotes:							

Company Name: Designed by:	Waber Consult Mahir Wa		County/City (Date:	20-Oct LWO21-00	55
Designed by:	Iviann vv	Design Volume	County/City	case ivo	LWQ21-00	33
Enter the are	a tributary to this facture			Λ -	0.37	narag
Effici the are	a tributary to this feature			$A_T =$	0.37	acres
Enter V _{BMP} o	determined from Section 2	.1 of this Handbook		$V_{BMP} =$	268	ft ³
	Type of B	Bioretention Facility	Design			
Side slopes re	equired (parallel to parking spaces o	r adjacent to walkways)				
O No side slope	s required (perpendicular to parking	space or Planter Boxes)				
	Bioreten	tion Facility Surface	Area			
Depth of Soi	l Filter Media Layer			$d_S =$	3.0	ft
					12.0	
Top Width o	f Bioretention Facility, ex	cluding curb		$\mathbf{w}_{\mathrm{T}} =$	13.0	ft
Total Effecti	ve Depth, d _E					
	$x d_S + (0.4) x 1 - (0.7/w_T)$	0 + 0.5		$d_E =$	1.75	ft
Minimum Sı	ırface Area, A _m					
	$\frac{V_{BMP}(ft^3)}{d_E(ft)}$	<u> </u>		$A_{M} =$	154	ft
	- \ /			۸ —	160	ft^2
Proposed Su	rrace Area			A=	168	π
	Biorete	ention Facility Prope	rties			
Side Slopes	in Bioretention Facility			$\mathbf{z} =$	4	:1
Diameter of	Underdrain				6	inches
Diameter of	Chachain			-	0	menes
Longitudinal	Slope of Site (3% maxim	um)			0.5	%
6" Check Da	m Spacing				0	feet

	Enter the are	a tributary t	o this feature			$A_{T} =$	0.19	acres
	Enter the are	a tributary t	to this feature			$A_T =$	0.19	acres
	Enter V _{BMP} o	letermined t	from Section 2	.1 of this Handbook		$V_{BMP} =$	144	ft ³
			Type of E	Bioretention Facility	Design			
ı	Side slopes re	quired (parallel	to parking spaces o	or adjacent to walkways)				
(_			space or Planter Boxes)				
			Bioreten	tion Facility Surface	e Area			
	Depth of Soi	l Filter Med				$d_S =$	3.0	ft
_	Depui of Soi	i i ilitoi ivico	na Layer			us	3.0	It
,	Top Width o	f Bioretenti	on Facility, ex	cluding curb		$\mathbf{w}_{\mathrm{T}} =$	15.0	ft
1	Total Effecti	va Danth d						
	Total Effection $d_{-} = (0.3)$	-	E) x 1 - (0.7/w _T)	1 + 0 5		$d_E = $	1.75	ft
	$\mathbf{u}_{\mathrm{E}} = (0.5)$	X us + (0.4)) X 1 (0.77 W ₁)	, 1 0.5		u _E	1.73	11
	Minimum Su	ırface Area.	A					
						$A_{M} =$	83	ft
	$A_{\rm M}$ (ft ⁻) =	V	$d_{E}(ft)$	_				
]	Proposed Su	rface Area				A=	98	ft ²
			D	4' E '1' D	··			
			Biorete	ention Facility Prope	erties			
,	Side Slopes i	n Bioretent	ion Facility			z =	4	:1
	Diameter of	Underdrain					6	inches
	Longitudinal	Slope of Si	ite (3% maxim	um)			0.5	%
(6" Check Da	m Spacing					0	feet
	Describe Veg		NT-4	ral Grasses				-
	Describe ve	retation:	Nam	rai Grasses				

Designed by:		Mahir Wa		County/City (case ino	LWQ21-00	55
			Design Volume				
Enter the	area tributary	to this feature			$A_T =$	0.46	acres
Enter V_{BN}	P determined	from Section 2	.1 of this Handbook		$V_{BMP} =$	786	ft ³
		Type of E	Bioretention Facility	Design			
_			or adjacent to walkways) g space or Planter Boxes)				
		Bioreten	tion Facility Surface	e Area			
Depth of S	Soil Filter Me	dia Layer			$d_S =$	3.0	ft
Top Widt	n of Bioretent	ion Facility, ex	cluding curb		$\mathbf{w}_{\mathrm{T}} =$	16.0	ft
	ctive Depth, $d_S = 0.2$	d _E 4) x 1 - (0.7/w _T)) + 0.5		$d_E = $	1.76	ft
	Surface Area V		_		$A_{M} = $	448	∫ft²
	Surface Area	-E ()			A=	454	ft^2
		Biorete	ention Facility Prope	erties			
Side Slop	es in Bioreten	tion Facility			$\mathbf{z} = $	4	:1
Diameter	of Underdrain	1				6	inches
Longitudi	nal Slope of S	Site (3% maxim	um)			0.5	%
6" Check	Dam Spacing					0	feet
	Vegetation:	NT /	ral Grasses				

Bioretention F	acility - Desi	on Procedure	BMP ID	Legend:	Require	ed Entries	
Dioretention	actifity - Design	gii i ioccduic	Basin 5	Legena.	Calcula	ated Cells	
Company Name:		Waber Consult			Date:	20-Oct	
Designed by:		Mahir Wa		County/City (Case No.:	LWQ21-00	55
			Design Volume				
Enter the	area tributary	to this feature			$A_T =$	1.21	acres
Enter V _B	MP determined	from Section 2.	.1 of this Handbook		$V_{BMP} =$	1,885	ft ³
		Type of B	Bioretention Facility	Design			
			r adjacent to walkways) space or Planter Boxes)				
		Bioreten	tion Facility Surface	e Area			
Depth of	Soil Filter Me	dia Layer			$d_S =$	3.0	ft
Top Wids	h of Bioretent	ion Facility, exc	cluding curb		$\mathbf{w}_{\mathrm{T}} =$	18.0	ft
	ective Depth, $d_{S} + (0.4)$	d _E 4) x 1 - (0.7/w _T)	+ 0.5		$d_E =$	1.76	ft
	Surface Area V		_		$A_{M} =$	1,071	ft ⁻
Proposed	Surface Area				A=	1,151	ft ²
		Biorete	ention Facility Prope	erties			
Side Slop	es in Bioreten	tion Facility			$\mathbf{z} =$	4	:1
Diameter	of Underdrair	ı				6	inches
Longitud	nal Slope of S	Site (3% maxim	um)			0.5	%
6" Check	Dam Spacing					0	feet
Describe	Vegetation:	Natur	ral Grasses				
Votes:							

Dia	retention Facil	ity Dogie	Procedure	BMP ID	Legend:	Require	ed Entries	
D 101	retention raci	iity - Desigi	1 Procedure	Basin 6	Legend.	Calcula	ited Cells	
_	ny Name:	7	Waber Consul	<u> </u>		Date:	20-Oct	
esigne	ed by:		Mahir W		County/City (Case No.:	LWQ21-00	55
				Design Volume				
	Enter the are	a tributary to	this feature			$A_T =$	0.14	acres
	Enter V _{BMP} d	etermined f	rom Section 2	.1 of this Handbook	Σ	$V_{BMP} =$	136	ft ³
			Type of E	Bioretention Facility	Design			
	Side slopes re	quired (parallel	o parking spaces o	or adjacent to walkways)				
	O No side slopes	required (perp	endicular to parking	space or Planter Boxes)				
			Bioreten	tion Facility Surfac	e Area			
	Danth of Coi	l Eilten Med		teron raciney Sarrac	-	a _	2.0	Ω
	Depth of Soi	i Filler Med	ia Layer			$d_S =$	3.0	ft
	Top Width o	f Bioretentio	on Facility, ex	cluding curb		$\mathbf{w}_{\mathrm{T}} =$	13.5	ft
	Total Effecti	ve Denth d						
			x 1 - (0.7/w _T)	0 + 0.5		$d_E = $	1.75	ft
	L ()	3 ()	(1)			L		
	Minimum Su	rface Area,	A_{m}					
	Λ (Ω^2) –	V _B	$_{MP}$ (ft ³)	_		$A_{M} = $	78	ft ⁻
			$_{\mathrm{E}}\left(\mathrm{ft}\right)$					2
	Proposed Sur	rface Area				A=	81	ft ²
			Biorete	ention Facility Prop	erties			
	Side Slopes i	n Bioretenti	on Facility			$\mathbf{z} =$	4	:1
	Diameter of	Underdrain					6	inche
								•
	Longitudinal	Slope of Si	te (3% maxim	um)			0.5	%
	6" Check Da	m Spacing					0	feet
	Describe Veg	getation:	Natu	ral Grasses				
otes:								

]	Enter V _{BMP} of	letermined fr	om Section 2	.1 of this Handbook		$V_{BMP} =$	136	ft ³
				Bioretention Facility				
					2 001611			
(_			or adjacent to walkways)				
) No side slope:	s required (perpe		g space or Planter Boxes)				
			Bioreten	tion Facility Surface	e Area			
]	Depth of Soi	l Filter Medi	a Layer			$d_S =$	3.0	ft
-	C 337: 141	£D:44:-	F 1114	-1 1'1-		*** =	12.0	C.
	lop wiath o	I Bioretentio	n Facility, ex	cluding curb		$\mathbf{w}_{\mathrm{T}} =$	12.0	ft
,	Total Effecti	ve Depth, d _E						
			x 1 - (0.7/w _T)) + 0.5		$d_E = $	1.74	ft
I	Minimum Su	ırface Area, A	\mathbf{A}_{m}					
	$\Delta_{r}(\mathbf{ft}^2) = 0$	V_{BM}	$_{\rm IP}$ (${\rm ft}^3$)	<u> </u>		$A_{M} = $	79	ft ⁻
-		_	(ft)				0.1	o.2
	Proposed Sur	rtace Area				A=	81	ft^2
			D					
			Biorete	ention Facility Prope	erties			
	Side Slopes i	in Bioretentic	on Facility			z =	4	:1
1	Diameter of	Undardrain					6	inches
j	Jianneter of	Underdrain					6	inches
]	Longitudinal	Slope of Sit	e (3% maxim	um)			0.5	%
,	6" Check Da	m Snacing				i	0	feet
		_					- 0	Iteet
	Describe Veg	actation.	Notus	ral Grasses				

Company Name:	Waber Consult	Basin 8		Date:	ted Cells 20-Oct	
Designed by:	Mahir Wa	· · · · · · · · · · · · · · · · · · ·	County/City (_		55
		Design Volume				
Enter the are	ea tributary to this feature			$A_T =$	0.3	acres
Enter V _{BMP}	determined from Section 2	.1 of this Handbook		$V_{BMP} =$	254	ft ³
	Type of B	Bioretention Facility	Design			
_	equired (parallel to parking spaces o es required (perpendicular to parking					
	Bioreten	tion Facility Surface	Area			
Depth of So	il Filter Media Layer			$d_S =$	3.0	ft
Top Width o	of Bioretention Facility, exc	cluding curb		$\mathbf{w}_{\mathrm{T}} =$	17.5	ft
	ive Depth, d_E $d_S = (0.4) \times 1 - (0.7/w_T)$	+ 0.5		$d_E =$	1.76	ft
	urface Area, A_{m} $\frac{V_{BMP} (ft^{3})}{d_{E} (ft)}$	_		$A_{M} = $	145	ft²
Proposed Su	- \ /			A=	149	ft ²
	Biorete	ention Facility Prope	rties			
Side Slopes	in Bioretention Facility			z =	4	:1
Diameter of	Underdrain				6	inches
	Slope of Site (3% maxim	um)			0.5	%
6" Check Da	m Spacing				0	feet
Describe Ve	getation: Natur	ral Grasses				

			<u>C</u>				
Entortho	araa tributarr	to this feature	Design Volume		$A_T =$	0.37	o orog
					237	0.57	acres
Enter V _{BM}	_{IP} determined	from Section 2	.1 of this Handbook		$V_{BMP} =$	275	ft ³
		Type of E	Bioretention Facility	Design			
Side slope	s required (paralle	el to parking spaces o	r adjacent to walkways)				
O No side sl	opes required (per	pendicular to parking	space or Planter Boxes)				
		Bioreten	tion Facility Surface	e Area			
Depth of S	Soil Filter Me				$d_S =$	3.0	ft
1		J			5		-
Top Widt	n of Bioretent	ion Facility, ex	cluding curb		$\mathbf{w}_{\mathrm{T}} =$	13.5	ft
Total Effa	ctive Depth, o	1					
	-	u _E 4) x 1 - (0.7/w _T)	1 + 0.5		$d_E = $	1.75	ft
₩ _E (¢) 11 05 (01	(01,7 11)			L	20,0	1.0
Minimum	Surface Area	. A					
					$A_{M} = $	158	ft-
$A_{\rm M}$ (It ²)) =V	$d_{E}(ft)$	_				
Proposed	Surface Area				A=	159	$\int ft^2$
		Biorete	ention Facility Prope	erties			
Side Slop	es in Bioreten	tion Facility			$\mathbf{z} =$	4	:1
1		J					-
Diameter	of Underdrain	1				6	inche
Longitudi	nal Slope of S	Site (3% maxim	um)			0.5	%
_	_		,				
6" Check	Dam Spacing					0	feet
			ral Grasses				

]	Longitudinal	Slope of Si	te (3% maxim	um)			0.5	%
	Diameter of						6	inches
	•					2		
	Side Slopes i	n Bioretent				z =	4	:1
			Biorete	ention Facility Prope	rties			
	rroposed Su	rrace Area				A^-	01	11
1	Proposed Su		$d_{E}(ft)$			A=	81	ft^2
]	Minimum Su $A_{1}(ft^{2}) =$	urface Area, V _E		_		$A_{M} = $	72	ft
	Total Effecti $d_E = (0.3)$	-	E) x 1 - (0.7/w _T)) + 0.5		$d_{\rm E} = $	1.75	ft
			on Facility, ex	cluding curb		$\mathbf{w}_{\mathrm{T}} =$	13.5	ft
	Depth of Soi		·			$d_S =$		ft
				tion Facility Surface	Area			
(No side slope:	s required (perp		space or Planter Boxes)				
(_			r adjacent to walkways)				
			Type of E	ioretention Facility	Design			
]	Enter V _{BMP} o	letermined 1	From Section 2	.1 of this Handbook		$V_{BMP} =$	124	ft ³
]	Enter the are	a tributary t	o this feature			$A_T =$	0.14	acres
	·			Design Volume	, ,	-		
esigned			Mahir Wa	· · · · · · · · · · · · · · · · · · ·	County/City (55
omponi	y Name:	,	Waber Consult	Basin 10		Calcula Date:	ted Cells 20-Oct	
Biore	etention Faci	lity - Desig	n Procedure	BMP ID	Legend:	_	ed Entries	

		Slope of Site (3					0.5	%
	Diameter of	Underdrain					6	inches
	Side Slopes i	in Bioretention F	Facility			z =	4	:1
			Biorete	ention Facility Prope	erties			
	Proposed Su	rface Area				A=	67	$\int ft^2$
	$A_{M}(ft^{2}) =$	$\frac{V_{\rm BMP}}{d_{\rm E}}$ (ft))	_		¹ M	07	
		urface Area, A _m	} ³)			$A_{M}=$	67	ft ⁻
		$x d_S + (0.4) x 1$	$-(0.7/w_T)$) + 0.5		$d_{E} = $	1.72	ft
	Total Effecti	ve Depth, d _E						
	Top Width o	f Bioretention F	acility, ex	cluding curb		$\mathbf{w}_{\mathrm{T}} =$	9.0	ft
	Depth of Soi	l Filter Media La	ayer			$d_S =$	3.0	ft
			Bioreten	tion Facility Surfac	e Area			
	O No side slopes	s required (perpendicu	ılar to parking	space or Planter Boxes)				
	Side slopes re	equired (parallel to par	king spaces o	or adjacent to walkways)				
			Type of E	Bioretention Facility	Design			
	Enter V _{BMP} o	letermined from	Section 2	.1 of this Handbook		$V_{BMP} =$	115	ft³
	Enter the are	a tributary to thi	s feature			$A_T =$	0.1	acres
				Design Volume		-		
Ompan Designe	y Name: d by:	vv au	Mahir Wa	<u> </u>	County/City			55
		, c	er Consult			Calcula Date:	ated Cells 20-Oct	
Bior	retention Faci	lity - Design Pro	ocedure	BMP ID Basin 11	Legend:		ed Entries ited Cells	

Dia	retention Facil	lity Docio	n Droceduro	BMP ID	Legend:	Require	ed Entries	
DIO	retention raci	iity - Desig	ii Procedure	Basin 12	Legena.	Calcula	ited Cells	
_	ny Name:	`	Waber Consult			Date:	20-Oct	
esigne	ed by:		Mahir Wa		County/City (Case No.:	LWQ21-00	55
				Design Volume				
	Enter the are	a tributary t	o this feature			$A_T =$	0.22	acres
	Enter V _{BMP} d	letermined f	From Section 2	.1 of this Handbook		$V_{BMP} =$	170	ft ³
			Type of E	Bioretention Facility	Design			
	Side slopes re	quired (parallel	to parking spaces o	or adjacent to walkways)				
	O No side slopes	required (perp	endicular to parking	space or Planter Boxes)				
			Bioreten	tion Facility Surface	e Area			
	Donth of Soi	l Filtor Mod		teres ruesticy surrues	11100	a –	3.0	ft
	Depth of Soi	i filler Med	lia Layei			$d_S =$	3.0	11
	Top Width o	f Bioretenti	on Facility, ex	cluding curb		$\mathbf{w}_{\mathrm{T}} =$	13.0	ft
	Total Effecti	ve Denth d	-					
			e) x 1 - (0.7/w _T)) + 0.5		$d_E = $	1.75	ft
	L ()	5 ()				2		
	Minimum Su	ırface Area,	$A_{\rm m}$					
	Λ (Ω^2) -	V _E	$_{MMP}$ (ft ³)			$A_{M} = $	98	ft
			$\mathbf{l}_{\mathrm{E}}\left(\mathbf{ft}\right)$					
	Proposed Sur	rface Area				A=	104	ft^2
	_		Biorete	ention Facility Prope	erties			
	Side Slopes i	n Bioretent	ion Facility			z =	4	:1
	are arepes .					-	•	
	Diameter of	Underdrain					6	inche
	Longitudinal	Slope of Si	te (3% maxim	um)			0.5	%
	6" Check Da	m Spacing					0	feet
	Describe Veg	getation:	Natu	ral Grasses				
otes:								

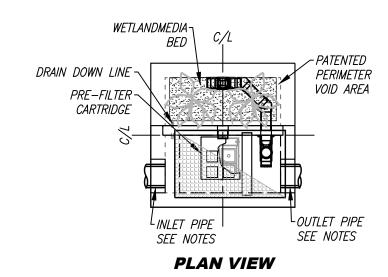
Designed	- J -		Mahir Wa	Design Volume	County/City			55
				Design Volume				
]	Enter the are	a tributary	to this feature			$A_T =$	0.31	acres
]	Enter V _{BMP} o	letermined	from Section 2	.1 of this Handbook		$V_{BMP} =$	285	ft ³
			Type of E	Bioretention Facility	Design			
(Side slopes re	quired (paralle	to parking spaces of	or adjacent to walkways)				
(_			space or Planter Boxes)				
			Bioreten	tion Facility Surface	e Area			
1	Depth of Soi	1 Filter Med			 	$d_S =$	3.0	ft
J	Depui of Soi	I TILLET WICE	na Layer			us	3.0	It
,	Гор Width o	f Bioretent	on Facility, ex	cluding curb		$\mathbf{w}_{\mathrm{T}} =$	13.5	ft
,	Гotal Effecti	ve Denth d	L					
		-	E) x 1 - (0.7/w _T)	0 + 0.5		$d_E = $	1.75	ft
	E (1-7)	3 (*	, (1)			L		
]	Minimum Su	ırface Area	, $A_{\rm m}$					
	$A_{\rm M}$ (ft ²) =	V	$\frac{1}{1}$ (C)			$A_{M} = $	164	ft²
1	Proposed Su		$d_{\rm E}$ (ft)			A=	192	ft^2
	Toposed Su.	race mea				71	172	11
			Biorete	ention Facility Prope	erties			
:	Side Slopes i	n Bioretent	ion Facility			$\mathbf{z} =$	4	:1
]	Diameter of	Underdrain					6	inches
								-
]	Longitudinal	Slope of S	ite (3% maxim	um)			0.5	%
(6" Check Da	m Spacing					0	feet
1	Describe Veg	ratation	Notu	ral Grasses		•		-
	Describe ve	getation.	Ivaiu.	iai Giasses				

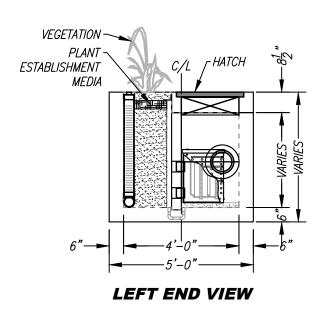
Enter the	e area tributary	to this feature			$A_T =$	0.15	acres
	•		.1 of this Handbook		$V_{BMP} =$		ft ³
		Type of E	Bioretention Facility	Design	_		_
(Side slo	pes required (paralle	el to parking spaces o	r adjacent to walkways)				
_			space or Planter Boxes)				
-		Bioreten	tion Facility Surface	e Area			
Denth of	Soil Filter Me			7 11 00	$d_S =$	3.0	ft
Deptil of	Son i mei we	dia Layer			uş	3.0	11
Top Wic	th of Bioretent	ion Facility, ex	cluding curb		$\mathbf{w}_{\mathrm{T}} =$	11.0	ft
Total Ff	fective Depth, o	1_					
		4) x 1 - (0.7/w _T)	0 + 0.5		$d_E = $	1.74	ft
L	, 5 .	, , , ,					
	n Surface Area						. 0.7
A _M (f	$\left(\frac{V}{V}\right) = \frac{V}{V}$	$\frac{f_{\rm BMP}({\rm ft}^3)}{1({\rm ft})}$	_		$A_{M} = $	119	ft ⁻
	d Surface Area	$\mathbf{d}_{\mathrm{E}}\left(\mathbf{\Pi}\right)$			A=	118	ft^2
•		rface area mu	st be equal to or gr	eater than the			
		D	d B W B	.•			
		Biorete	ention Facility Prope	rties			
Side Slo	pes in Bioreten	tion Facility			z =	4	:1
	r of Underdrain	1				6	inches
Diamete							_
Diamete			um)			0.5	%
	linal Slope of S	Site (3% maxim	uiii)				
Longitud	linal Slope of S c Dam Spacing		um)			0	feet
Longitud	_		ral Grasses			0	feet

Dioretention Faci	lity - Design Procedure	BMP ID	Legend:	Require	ed Entries	
Bioretennon raci	inty - Design Procedure	Basin 15	Legena.	Calcula	ated Cells	
Company Name:	Waber Consult	· · · · · · · · · · · · · · · · · · ·		Date:	20-Oct	
Designed by:	Mahir Wa		County/City	Case No.:	LWQ21-00	55
		Design Volume				
Enter the are	ea tributary to this feature			$A_T =$	0.24	acres
Enter V _{BMP} o	determined from Section 2	.1 of this Handbook		$V_{BMP} =$	417	ft ³
	Type of B	Bioretention Facility	Design			
<u>_</u>	equired (parallel to parking spaces on sequired (perpendicular to parking					
	Bioreten	tion Facility Surface	e Area			
Depth of Soi	il Filter Media Layer			$d_S =$	3.0	ft
Top Width o	of Bioretention Facility, ex-	cluding curb		$\mathbf{w}_{\mathrm{T}} =$	11.5	ft
	ve Depth, d_E x $d_S + (0.4) \times 1 - (0.7/w_T)$) + 0.5		$d_E =$	1.74	ft
	urface Area, A_{m} $V_{BMP} (ft^{3})$ $d_{E} (ft)$	_		$A_{M} =$	240	ft
Proposed Su	2 ()			A=	238	ft^2
ERROR, the p	roposed surface area mu	st be equal to or gro	eater than the	minimur	m surface a	rea
	Biorete	ention Facility Prope	rties			
Side Slopes	in Bioretention Facility			$_{\mathrm{Z}}$ =	4	:1
Diameter of	Underdrain				6	inche
Longitudinal	Slope of Site (3% maxim	um)			0.5	%
6" Check Da	um Spacing				0	feet
		1.0				
Describe Ve	getation: Natu	ral Grasses				

Total Effective Depth, d_E $d_E = (0.3) \times d_S + (0.4) \times 1 - (0.7/w_T) + 0.5$ $d_E = 1.74 \text{ ft}$ Minimum Surface Area, A_m $A_M (ft^2) = \frac{V_{BMP} (ft^3)}{d_E (ft)}$ $Proposed Surface Area$ $A = 97 \text{ ft}^2$ Bioretention Facility Properties Side Slopes in Bioretention Facility $z = 4 \text{ :1}$ Diameter of Underdrain $c = 0.5 \text{ %}$ $c = 0.5 \text$	1 op William o	of Bioretention Facility, ex	eruam B care		$\mathbf{w}_{\mathrm{T}} =$	12.5	ft
$d_{E} = (0.3) \times d_{S} + (0.4) \times 1 - (0.7/w_{T}) + 0.5$ $d_{E} = 1.74 \text{ ft}$ Minimum Surface Area, A_{m} $A_{M} (ft^{2}) = \frac{V_{BMP} (ft^{3})}{d_{E} (ft)}$ Proposed Surface Area $A = 97 \text{ ft}^{2}$ Bioretention Facility Properties Side Slopes in Bioretention Facility $z = 4 : 1$ Diameter of Underdrain $Longitudinal Slope of Site (3% maximum)$ $6" \text{ Check Dam Spacing}$ 0 feet							-
$d_{E} = (0.3) \times d_{S} + (0.4) \times 1 - (0.7/w_{T}) + 0.5$ $d_{E} = 1.74 \text{ ft}$ Minimum Surface Area, A_{m} $A_{M} (ft^{2}) = \frac{V_{BMP} (ft^{3})}{d_{E} (ft)}$ Proposed Surface Area $A = 97 \text{ ft}^{2}$ Bioretention Facility Properties Side Slopes in Bioretention Facility $z = 4 : 1$ Diameter of Underdrain $Longitudinal Slope of Site (3% maximum)$ $6" \text{ Check Dam Spacing}$ 0 feet	Total Effecti	va Danth d					
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$\begin{array}{c} \text{Minimum Surface Area, A}_m \\ A_M (\text{ft}^2) = \frac{V_{\text{BMP}} (\text{ft}^3)}{d_E (\text{ft})} \\ \text{Proposed Surface Area} \\ \hline \\ & Bioretention Facility Properties} \\ \\ \text{Side Slopes in Bioretention Facility} \\ & z = \underbrace{\begin{array}{c} 4 \\ \text{:1} \end{array}}_{\text{Inches}} \\ \\ \text{Longitudinal Slope of Site (3\% maximum)} \\ \\ 6" \text{Check Dam Spacing} \\ \hline \end{array}$	$d_{\rm E} = (0.3)$	$x d_S + (0.4) x 1 - (0.7/w_T)$	+0.5		$d_{\rm E} = $	1.74	ft
$A_{M} (ft^{2}) = \frac{V_{BMP} (ft^{3})}{d_{E} (ft)}$ Proposed Surface Area $A = 97 ft^{2}$ Bioretention Facility Properties $z = 4 :1$ Diameter of Underdrain $Longitudinal Slope of Site (3% maximum)$ $6" Check Dam Spacing$ $0 feet$	\mathbf{u}_{E} (0.3)	(((((((((((((((((((, , 0.3		u _E	1.71	111
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Bioretention Facility Properties Side Slopes in Bioretention Facility $z = 4$:1 Diameter of Underdrain 6 inches Longitudinal Slope of Site (3% maximum) 0.5 % 6" Check Dam Spacing 0 feet		- \ /			A=	97	ft^2
Side Slopes in Bioretention Facility $z = 4$:1 Diameter of Underdrain 6 inches Longitudinal Slope of Site (3% maximum) 0.5 % 6" Check Dam Spacing 0 feet	Troposed Bu	Trace Area			Α	<i>)</i>	11
Side Slopes in Bioretention Facility $z = 4$:1 Diameter of Underdrain 6 inches Longitudinal Slope of Site (3% maximum) 0.5 % 6" Check Dam Spacing 0 feet							
Side Slopes in Bioretention Facility $z = 4$:1 Diameter of Underdrain 6 inches Longitudinal Slope of Site (3% maximum) 0.5 % 6" Check Dam Spacing 0 feet							
Side Slopes in Bioretention Facility $z = 4$:1 Diameter of Underdrain 6 inches Longitudinal Slope of Site (3% maximum) 0.5 % 6" Check Dam Spacing 0 feet	_	Biorete	ention Facility Prope	rties			
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Longitudinal Slope of Site (3% maximum) 6" Check Dam Spacing 0 feet	D: 0						
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6" Check Dam Spacing 0 feet					-		-
6" Check Dam Spacing 0 feet	Longitudinal	Slana of Sita (20/2 maxim	um)			0.5	0/2
	Longitudinal	i Stope of Site (3% maxim	um)			0.5	7 0
	6" Chaole Da	m Snaaina				0	foot
Describe Vegetation: Natural Grasses	6" Check Da	m Spacing				0	teet
Describe Vegetation: Natural Grasses	_ "		1.0				
			1.0				

SITE SPECIFIC DATA				
PROJECT NUMBER				
PROJECT NAME				
PROJECT LOCATI	ION			
STRUCTURE ID				
	TREATMENT	REQUIRED		
VOLUME B	ASED (CF)	FLOW BAS	SED (CFS)	
N,	/A			
PEAK BYPASS R	PEQUIRED (CFS) —	IF APPLICABLE		
PIPE DATA	I.E.	MATERIAL	DIAMETER	
INLET PIPE 1				
INLET PIPE 2				
OUTLET PIPE				
	PRETREATMENT	BIOFILTRATION	DISCHARGE	
RIM ELEVATION				
SURFACE LOAD				
FRAME & COVER	24" X 42"		N/A	



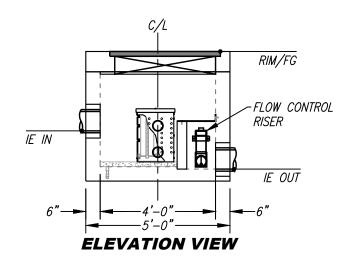


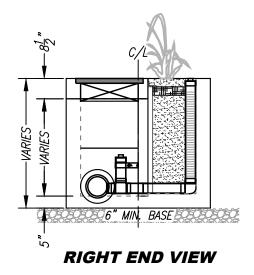
INSTALLATION NOTES

- 1. CONTRACTOR TO PROVIDE ALL LABOR, EQUIPMENT, MATERIALS AND INCIDENTALS REQUIRED TO OFFLOAD AND INSTALL THE SYSTEM AND APPURTENANCES IN ACCORDANCE WITH THIS DRAWING AND THE MANUFACTURERS SPECIFICATIONS, UNLESS OTHERWISE STATED IN MANUFACTURERS CONTRACT.
- 2. UNIT MUST BE INSTALLED ON LEVEL BASE. MANUFACTURER
 RECOMMENDS A MINIMUM 6" LEVEL ROCK BASE UNLESS SPECIFIED BY
 THE PROJECT ENGINEER. CONTRACTOR IS RESPONSIBLE TO VERIFY
 PROJECT ENGINEERS RECOMMENDED BASE SPECIFICATIONS.
- 4. CONTRACTOR TO SUPPLY AND INSTALL ALL EXTERNAL CONNECTING PIPES. ALL PIPES MUST BE FLUSH WITH INSIDE SURFACE OF CONCRETE. (PIPES CANNOT INTRUDE BEYOND FLUSH). INVERT OF OUTFLOW PIPE MUST BE FLUSH WITH DISCHARGE CHAMBER FLOOR. ALL PIPES SHALL BE SEALED WATER TIGHT PER MANUFACTURERS STANDARD CONNECTION DETAIL.
- 5. CONTRACTOR RESPONSIBLE FOR INSTALLATION OF ALL RISERS, MANHOLES, AND HATCHES. CONTRACTOR TO GROUT ALL MANHOLES AND HATCHES TO MATCH FINISHED SURFACE UNLESS SPECIFIED OTHERWISE.
- 6. VEGETATION SUPPLIED AND INSTALLED BY OTHERS. ALL UNITS WITH VEGETATION MUST HAVE DRIP OR SPRAY IRRIGATION SUPPLIED AND INSTALLED BY OTHERS.
- 7. CONTRACTOR RESPONSIBLE FOR CONTACTING BIO CLEAN FOR ACTIVATION OF UNIT. MANUFACTURERS WARRANTY IS VOID WITH OUT PROPER ACTIVATION BY A BIO CLEAN REPRESENTATIVE.

GENERAL NOTES

- 1. MANUFACTURER TO PROVIDE ALL MATERIALS UNLESS OTHERWISE NOTED.
- 2. ALL DIMENSIONS, ELEVATIONS, SPECIFICATIONS AND CAPACITIES ARE SUBJECT TO CHANGE. FOR PROJECT SPECIFIC DRAWINGS DETAILING EXACT DIMENSIONS, WEIGHTS AND ACCESSORIES PLEASE CONTACT BIO CLEAN.





WETLAND MEDIA LOADING RATE (GPM/SF)	
PRETREATMENT LOADING RATE (GPM/SF)	
OPERATING HEAD (FT)	
TREATMENT FLOW (CFS)	

THIS PRODUCT MAY BE PROTECTED BY ONE OR MORE OF THE FOLLOWING US PATENTS: 7,425,262; 7,470,362; 7,674,376; 8,303,616; RELATED FOREIGN PATENTS OR OTHER PATENTS PENDING

PROPRIETARY AND CONFIDENTIAL:

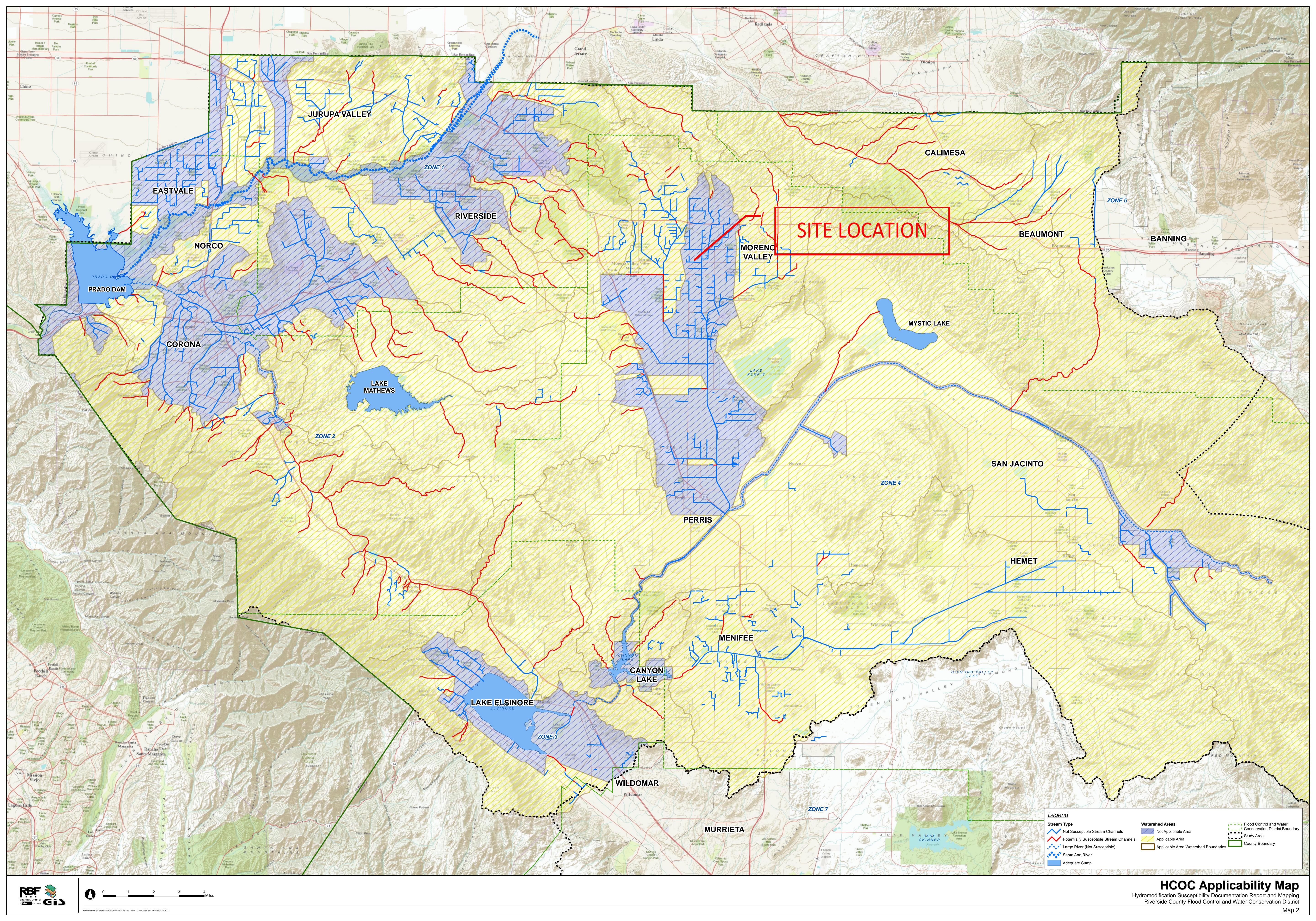
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MWS-L-4-4-V STORMWATER BIOFILTRATION SYSTEM STANDARD DETAIL

Appendix 7: Hydromodification

Supporting Detail Relating to Hydrologic Conditions of Concern



Appendix 8: Source Control

Pollutant Sources/Source Control Checklist

How to use this worksheet (also see instructions in Section G of the WQMP Template):

- 1. Review Column 1 and identify which of these potential sources of stormwater pollutants apply to your site. Check each box that applies.
- 2. Review Column 2 and incorporate all of the corresponding applicable BMPs in your WQMP Exhibit.
- 3. Review Columns 3 and 4 and incorporate all of the corresponding applicable permanent controls and operational BMPs in your WQMP. Use the format shown in Table G.1on page 23 of this WQMP Template. Describe your specific BMPs in an accompanying narrative, and explain any special conditions or situations that required omitting BMPs or substituting alternative BMPs for those shown here.

	E SOURCES WILL BE PROJECT SITE	THEN YOUR WQMP SH	OULI	D INCLUDE THESE SOURCE CONT	ROL	. BMPs, AS APPLICABLE
	1 Intential Sources of Runoff Pollutants	2 Permanent Controls—Show on WQMP Drawings	Pei	3 rmanent Controls—List in WQMP Table and Narrative	Op	4 perational BMPs—Include in WQMP Table and Narrative
Ø	A. On-site storm drain inlets	Locations of inlets.	X	Mark all inlets with the words "Only Rain Down the Storm Drain" or similar. Catch Basin Markers may be available from the Riverside County Flood Control and Water Conservation District, call 951.955.1200 to verify.	M D M D	Maintain and periodically repaint or replace inlet markings. Provide stormwater pollution prevention information to new site owners, lessees, or operators. See applicable operational BMPs in Fact Sheet SC-44, "Drainage System Maintenance," in the CASQA Stormwater Quality Handbooks at www.cabmphandbooks.com Include the following in lease agreements: "Tenant shall not allow anyone to discharge anything to storm drains or to store or deposit materials so as to create a potential discharge to storm drains."
	B. Interior floor drains and elevator shaft sump pumps			State that interior floor drains and elevator shaft sump pumps will be plumbed to sanitary sewer.		Inspect and maintain drains to prevent blockages and overflow.
	C. Interior parking garages			State that parking garage floor drains will be plumbed to the sanitary sewer.		Inspect and maintain drains to prevent blockages and overflow.

IF THESE SOURCES WILL BE ON THE PROJECT SITE			THEN YOUR WQMP SHOULD INCLUDE THESE SOURCE CONTROL BMPs, AS APPLICABLE				
1 Potential Sources of Runoff Pollutants		2 Permanent Controls—Show on WQMP Drawings		Per	3 manent Controls—List in WQMP Table and Narrative	4 Operational BMPs—Include in WQM Table and Narrative	
X	D1. Need for future indoor & structural pest control			M	Note building design features that discourage entry of pests.	×	Provide Integrated Pest Management information to owners, lessees, and operators.
⊠	D2. Landscape/ Outdoor Pesticide Use		Show locations of native trees or areas of shrubs and ground cover to be undisturbed and retained. Show self-retaining landscape areas, if any. Show stormwater treatment and hydrograph modification management BMPs. (See instructions in Chapter 3, Step 5 and guidance in Chapter 5.)		State that final landscape plans will accomplish all of the following. Preserve existing native trees, shrubs, and ground cover to the maximum extent possible. Design landscaping to minimize irrigation and runoff, to promote surface infiltration where appropriate, and to minimize the use of fertilizers and pesticides that can contribute to stormwater pollution. Where landscaped areas are used to retain or detain stormwater, specify plants that are tolerant of saturated soil conditions. Consider using pest-resistant plants, especially adjacent to hardscape. To insure successful establishment, select plants appropriate to site soils, slopes, climate, sun, wind, rain, land use, air movement, ecological consistency, and plant interactions.		Maintain landscaping using minimu or no pesticides. See applicable operational BMPs in "What you should know forLandscape and Gardening" at http://rcflood.org/stormwater/Error! Hyperlink reference not valid. Provide IPM information to new owners, lessees and operators.

	E SOURCES WILL BE PROJECT SITE		THEN YOUR WQMP SHO	DULE) INCLUDE THESE SOURCE CONT	ROL	BMPs, AS APPLICABLE
	1 tential Sources of Runoff Pollutants	F	2 Permanent Controls—Show on WQMP Drawings	Per	3 rmanent Controls—List in WQMP Table and Narrative	Op	4 perational BMPs—Include in WQMP Table and Narrative
	E. Pools, spas, ponds, decorative fountains, and other water features.		Show location of water feature and a sanitary sewer cleanout in an accessible area within 10 feet. (Exception: Public pools must be plumbed according to County Department of Environmental Health Guidelines.)		If the Co-Permittee requires pools to be plumbed to the sanitary sewer, place a note on the plans and state in the narrative that this connection will be made according to local requirements.		See applicable operational BMPs in "Guidelines for Maintaining Your Swimming Pool, Jacuzzi and Garden Fountain" at http://rcflood.org/stormwater/
	F. Food service		For restaurants, grocery stores, and other food service operations, show location (indoors or in a covered area outdoors) of a floor sink or other area for cleaning floor mats, containers, and equipment. On the drawing, show a note that this drain will be connected to a grease interceptor before discharging to the sanitary sewer.	<u> </u>	Describe the location and features of the designated cleaning area. Describe the items to be cleaned in this facility and how it has been sized to insure that the largest items can be accommodated.		See the brochure, "The Food Service Industry Best Management Practices for: Restaurants, Grocery Stores, Delicatessens and Bakeries" at http://rcflood.org/stormwater/ Provide this brochure to new site owners, lessees, and operators.
⊠ (G. Refuse areas	× ·	Show where site refuse and recycled materials will be handled and stored for pickup. See local municipal requirements for sizes and other details of refuse areas. If dumpsters or other receptacles are outdoors, show how the designated area will be covered, graded, and paved to prevent runon and show locations of berms to prevent runoff from the area. Any drains from dumpsters, compactors, and tallow bin areas shall be connected to a grease removal device before discharge to sanitary sewer.	DX DX	State how site refuse will be handled and provide supporting detail to what is shown on plans. State that signs will be posted on or near dumpsters with the words "Do not dump hazardous materials here" or similar.	×	State how the following will be implemented: Provide adequate number of receptacles. Inspect receptacles regularly; repair or replace leaky receptacles. Keep receptacles covered. Prohibit/prevent dumping of liquid or hazardous wastes. Post "no hazardous materials" signs. Inspect and pick up litter daily and clean up spills immediately. Keep spill control materials available on-site. See Fact Sheet SC-34, "Waste Handling and Disposal" in the CASQA Stormwater Quality Handbooks at www.cabmphandbooks.com

IF THESE SOURCES WILL BE ON THE PROJECT SITE	THEN YOUR WQMP SH	OULD INCLUDE THESE SOURCE CONT	ROL BMPs, AS APPLICABLE
1 Potential Sources of Runoff Pollutants	2 Permanent Controls—Show on WQMP Drawings	3 Permanent Controls—List in WQMP Table and Narrative	4 Operational BMPs—Include in WQMP Table and Narrative
☐ H. Industrial processes.	☐ Show process area.	☐ If industrial processes are to be located on site, state: "All process activities to be performed indoors. No processes to drain to exterior or to storm drain system."	See Fact Sheet SC-10, "Non-Stormwater Discharges" in the CASQA Stormwater Quality Handbooks at www.cabmphandbooks.com See the brochure "Industrial & Commercial Facilities Best Management Practices for: Industrial, Commercial Facilities" at http://rcflood.org/stormwater/

IF THESE SOURCES WILL BE ON THE PROJECT SITE	THEN YOUR WQMP SHO	OULD INCLUDE THESE SOURCE CONT	ROL BMPs, AS APPLICABLE
1 Potential Sources of Runoff Pollutants	2 Permanent Controls—Show on WQMP Drawings	3 Permanent Controls—List in WQMP Table and Narrative	4 Operational BMPs—Include in WQMP Table and Narrative
I. Outdoor storage of equipment or materials. (See rows J and K for source control measures for vehicle cleaning, repair, and maintenance.)	 Show any outdoor storage areas, including how materials will be covered. Show how areas will be graded and bermed to prevent runon or run-off from area. Storage of non-hazardous liquids shall be covered by a roof and/or drain to the sanitary sewer system, and be contained by berms, dikes, liners, or vaults. Storage of hazardous materials and wastes must be in compliance with the local hazardous materials ordinance and a Hazardous Materials Management Plan for the site. 	Include a detailed description of materials to be stored, storage areas, and structural features to prevent pollutants from entering storm drains. Where appropriate, reference documentation of compliance with the requirements of Hazardous Materials Programs for: Hazardous Waste Generation Hazardous Materials Release Response and Inventory California Accidental Release (CalARP) Aboveground Storage Tank Uniform Fire Code Article 80 Section 103(b) & (c) 1991 Underground Storage Tank	See the Fact Sheets SC-31, "Outdoor Liquid Container Storage" and SC-33, "Outdoor Storage of Raw Materials" in the CASQA Stormwater Quality Handbooks at www.cabmphandbooks.com

IF THESE SOURCES WILL BE ON THE PROJECT SITE	THEN YOUR WQMP SHO	DULD INCLUDE THESE SOURCE CONT	ROL BMPs, AS APPLICABLE
1 Potential Sources of Runoff Pollutants	2 Permanent Controls—Show on WQMP Drawings	3 Permanent Controls—List in WQMP Table and Narrative	4 Operational BMPs—Include in WQMP Table and Narrative
J. Vehicle and Equipment Cleaning	☐ Show on drawings as appropriate: (1) Commercial/industrial facilities having vehicle/equipment cleaning needs shall either provide a covered, bermed area for washing activities or discourage vehicle/equipment washing by removing hose bibs and installing signs prohibiting such uses. (2) Multi-dwelling complexes shall have a paved, bermed, and covered car wash area (unless car washing is prohibited on-site and hoses are provided with an automatic shutoff to discourage such use). (3) Washing areas for cars, vehicles, and equipment shall be paved, designed to prevent run-on to or runoff from the area, and plumbed to drain to the sanitary sewer. (4) Commercial car wash facilities shall be designed such that no runoff from the facility is discharged to the storm drain system. Wastewater from the facility shall discharge to the sanitary sewer, or a wastewater reclamation system shall be installed.	If a car wash area is not provided, describe any measures taken to discourage on-site car washing and explain how these will be enforced.	Describe operational measures to implement the following (if applicable): Washwater from vehicle and equipment washing operations shall not be discharged to the storm drain system. Refer to "Outdoor Cleaning Activities and Professional Mobile Service Providers" for many of the Potential Sources of Runoff Pollutants categories below. Brochure can be found at http://rcflood.org/stormwater/ Car dealerships and similar may rinse cars with water only.

IF THESE SOURCES WILL BE ON THE PROJECT SITE	THEN YOUR WQMP SHO	OULD INCLUDE THESE SOURCE CONT	ROL BMPs, AS APPLICABLE
1 Potential Sources of Runoff Pollutants	2 Permanent Controls—Show on WQMP Drawings	3 Permanent Controls—List in WQMP Table and Narrative	4 Operational BMPs—Include in WQMP Table and Narrative
K. Vehicle/Equipment Repair and Maintenance	 □ Accommodate all vehicle equipment repair and maintenance indoors. Or designate an outdoor work area and design the area to prevent run-on and runoff of stormwater. □ Show secondary containment for exterior work areas where motor oil, brake fluid, gasoline, diesel fuel, radiator fluid, acid-containing batteries or other hazardous materials or hazardous wastes are used or stored. Drains shall not be installed within the secondary containment areas. □ Add a note on the plans that states either (1) there are no floor drains, or (2) floor drains are connected to wastewater pretreatment systems prior to discharge to the sanitary sewer and an industrial waste discharge permit will be obtained. 	□ State that no vehicle repair or maintenance will be done outdoors, or else describe the required features of the outdoor work area. □ State that there are no floor drains or if there are floor drains, note the agency from which an industrial waste discharge permit will be obtained and that the design meets that agency's requirements. □ State that there are no tanks, containers or sinks to be used for parts cleaning or rinsing or, if there are, note the agency from which an industrial waste discharge permit will be obtained and that the design meets that agency's requirements.	In the Stormwater Control Plan, note that all of the following restrictions apply to use the site: No person shall dispose of, nor permit the disposal, directly or indirectly of vehicle fluids, hazardous materials, or rinsewater from parts cleaning into storm drains. No vehicle fluid removal shall be performed outside a building, nor on asphalt or ground surfaces, whether inside or outside a building, except in such a manner as to ensure that any spilled fluid will be in an area of secondary containment. Leaking vehicle fluids shall be contained or drained from the vehicle immediately. No person shall leave unattended drip parts or other open containers containing vehicle fluid, unless such containers are in use or in an area of secondary containment. Refer to "Automotive Maintenance & Car Care Best Management Practices for Auto Body Shops, Auto Repair Shops, Car Dealerships, Gas Stations and Fleet Service Operations". Brochure can be found at http://rcflood.org/stormwater/ Refer to Outdoor Cleaning Activities and Professional Mobile Service Providers for many of the Potential Sources of Runoff Pollutants categories below. Brochure can be found at http://rcflood.org/stormwater/

IF THESE SOURCES WILL BE ON THE PROJECT SITE	THEN YOUR WQMP SHO	OULD INCLUDE THESE SOURCE CONT	ROL BMPs, AS APPLICABLE
1 Potential Sources of Runoff Pollutants	2 Permanent Controls—Show on WQMP Drawings	3 Permanent Controls—List in WQMP Table and Narrative	4 Operational BMPs—Include in WQMP Table and Narrative
L. Fuel Dispensing Areas	□ Fueling areas ⁶ shall have impermeable floors (i.e., portland cement concrete or equivalent smooth impervious surface) that are: a) graded at the minimum slope necessary to prevent ponding; and b) separated from the rest of the site by a grade break that prevents run-on of stormwater to the maximum extent practicable. □ Fueling areas shall be covered by a canopy that extends a minimum of ten feet in each direction from each pump. [Alternative: The fueling area must be covered and the cover's minimum dimensions must be equal to or greater than the area within the grade break or fuel dispensing area ¹ .] The canopy [or cover] shall not drain onto the fueling area.		□ The property owner shall dry sweep the fueling area routinely. □ See the Fact Sheet SD-30, "Fueling Areas" in the CASQA Stormwater Quality Handbooks at www.cabmphandbooks.com

⁶ The fueling area shall be defined as the area extending a minimum of 6.5 feet from the corner of each fuel dispenser or the length at which the hose and nozzle assembly may be operated plus a minimum of one foot, whichever is greater.

	SE SOURCES WILL BE E PROJECT SITE	THEN YOUR WQMP SHO	OULD INCLUDE THESE SOURCE CONT	ROL BMPs, AS APPLICABLE
	1 otential Sources of Runoff Pollutants	2 Permanent Controls—Show on WQMP Drawings	3 Permanent Controls—List in WQMP Table and Narrative	4 Operational BMPs—Include in WQMP Table and Narrative
	M. Loading Docks	Show a preliminary design for the loading dock area, including roofing and drainage. Loading docks shall be covered and/or graded to minimize run-on to and runoff from the loading area. Roof downspouts shall be positioned to direct stormwater away from the loading area. Water from loading dock areas shall be drained to the sanitary sewer, or diverted and collected for ultimate discharge to the sanitary sewer.		 ■ Move loaded and unloaded items indoors as soon as possible. ■ See Fact Sheet SC-30, "Outdoor Loading and Unloading," in the CASQA Stormwater Quality Handbooks at www.cabmphandbooks.com
		 □ Loading dock areas draining directly to the sanitary sewer shall be equipped with a spill control valve or equivalent device, which shall be kept closed during periods of operation. □ Provide a roof overhang over the loading area or install door skirts (cowling) at each bay that enclose the end of the trailer. 		

SE SOURCES WILL BE PROJECT SITE	THEN YOUR WQMP SHOULD INCLUDE THESE SOURCE CONTROL BMPs, AS APPLICABLE			
1 Itential Sources of Runoff Pollutants	2 Permanent Controls—Show on WQMP Drawings	3 Permanent Controls—List in WQMP Table and Narrative	4 Operational BMPs—Include in WQMP Table and Narrative	
N. Fire Sprinkler Test Water		Provide a means to drain fire sprinkler test water to the sanitary sewer.	□ See the note in Fact Sheet SC-41, "Building and Grounds Maintenance," in the CASQA Stormwater Quality Handbooks at www.cabmphandbooks.com	
O. Miscellaneous Drain or Wash Water or Other Sources Boiler drain lines Condensate drain lines Rooftop equipment Drainage sumps Roofing, gutters, and trim. Other sources		Boiler drain lines shall be directly or indirectly connected to the sanitary sewer system and may not discharge to the storm drain system. Condensate drain lines may discharge to landscaped areas if the flow is small enough that runoff will not occur. Condensate drain lines may not discharge to the storm drain system. Rooftop equipment with potential to produce pollutants shall be roofed and/or have secondary containment. Any drainage sumps on-site shall feature a sediment sump to reduce the quantity of sediment in pumped water. Avoid roofing, gutters, and trim made of copper or other unprotected metals that may leach into runoff. Include controls for other sources as specified by local reviewer.		

IF THESE SOURCES WILL BE ON THE PROJECT SITE	THEN YOUR WQMP SHOULD INCLUDE THESE SOURCE CONTROL BMPs, AS APPLICABLE		
1 Potential Sources of Runoff Pollutants	2 Permanent Controls—Show on WQMP Drawings	3 Permanent Controls—List in WQMP Table and Narrative	4 Operational BMPs—Include in WQMP Table and Narrative
P. Plazas, sidewalks, and parking lots.			Sweep plazas, sidewalks, and parking lots regularly to prevent accumulation of litter and debris. Collect debris from pressure washing to prevent entry into the storm drain system. Collect washwater containing any cleaning agent or degreaser and discharge to the sanitary sewer not to a storm drain.

Appendix 9: O&M

Operation and Maintenance Plan and Documentation of Finance, Maintenance and Recording Mechanisms

Appendix 10: Educational Materials

BMP Fact Sheets, Maintenance Guidelines and Other End-User BMP Information